HEALTH TECHNICAL MEMORANDUM 2010
Sterilization
Part 5: Good practice guide
1995

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Part 5: Good practice guide

Sterilization

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Health Technical Memoranda (HTMs) give comprehensive advice and guidance on the design, installation and operation of specialised building and engineering technology used in the delivery of healthcare.

They are applicable to new and existing sites, and are for use at various stages during the inception, design, construction, refurbishment and maintenance of a building.

Health Technical Memorandum 2010

HTM 2010 is being published in five parts:

- **Part 1 - Management policy** - is a summary of the information required by non-technical personnel responsible for the management of sterilization services. It discusses the various types of sterilizer, for both clinical and laboratory use, and also contains guidance on legal and policy matters, and on the appointment and responsibilities of personnel. It should be read by anyone consulting this memorandum for the first time;

- **Part 2 - Design considerations** - contains information relevant to the specification and installation of new sterilizing equipment. It discusses the requirements for each type of sterilizer and outlines the specifications to be included in any contract. Practical considerations for the installation of sterilizers are discussed, including siting, heat emission, ventilation, noise and vibration, and mains services with an emphasis on steam quality;

- **Part 3 - Validation and verification** - covers all aspects of validation and periodic testing of sterilizers. It includes detailed schedules and procedures for tests and checks to be carried out for commissioning and performance qualification, and for subsequent periodic testing;

- **Part 4 - Operational management** - covers all aspects of the routine operation and maintenance of sterilizers, stressing the need for a planned
maintenance programme along with the type of records to be kept. Advice on the safe and efficient operation of sterilizers is given, as well as procedures for reporting defects and accidents;

• Part 5 - Good practice guide - provides advice on the fatigue life of pressure vessels, the lethality of heat sterilization processes, steam, contracts for testing, and accommodation for gas cylinders and canisters. It also includes a comprehensive bibliography.

The contents of this HTM in terms of management policy and operational policy are endorsed by:

a. the Welsh Office for the NHS in Wales;

b. the Health and Personal Social Services Management Executive in Northern Ireland;

c. the National Health Service in Scotland Management Executive.

References to legislation appearing in the main text of this guidance apply to the United Kingdom as a whole, except where marginal notes indicate variations for Scotland and Northern Ireland. Where appropriate, marginal notes are also used to amplify the text.
Preface

HTM 2010 gives guidance on the choice, specification, purchase, installation, validation, periodic testing, operation and maintenance of the following types of sterilizer in use in the National Health Service:

a. clinical sterilizers:
   (i) high-temperature steam sterilizers used for processing porous loads (including instruments and utensils wrapped in porous materials);
   (ii) high-temperature steam sterilizers used for processing aqueous fluids in sealed containers;
   (iii) high-temperature steam sterilizers used for processing unwrapped solid instruments and utensils;
   (iv) dry-heat sterilizers (hot-air sterilizers);
   (v) low-temperature steam (LTS) disinfectors and low-temperature steam and formaldehyde (LTSF) sterilizers;
   (vi) ethylene oxide (EO) sterilizers;

b. laboratory sterilizers:
   (i) high-temperature steam sterilizers used with one or more specialised operating cycles;
   (ii) culture media preparators.

No guidance is given on sterilization by irradiation, hydrogen peroxide, gas plasma or filtration. Users who wish to employ these processes bear the responsibility of ensuring that the validation procedures comply with the principles outlined in Part 3 of this HTM and that the intended operating procedures will ensure an efficacious process for the different types of load.

This HTM is intended primarily as a guide for technical personnel, whether specialists in sterilizers and sterilization procedures or those responsible for maintenance and testing. It is also intended for those responsible for the day-to-day running of sterilizers, and will also be of interest to supplies officers, architects, estates managers and others in both the public and private sectors.

Detailed information on the planning and design of a sterile services department, including the level of provision of sterilizers, is given in Health Building Note 13, ‘Sterile services department’. Guidance for laboratory installations can be found in Health Building Note 15, ‘Accommodation for pathology services’.

Although this edition of HTM 2010 reflects established sterilizer technology, it is recognised that considerable scope exists for the utilisation of emerging technology in the management of sterilizers. This will be kept under review with the aim of introducing recommendations for such technology at the earliest opportunity so that the procedures essential for the efficient, safe and effective operation of sterilizers can be optimised.

Most of the British Standards for sterilizers which were applicable at the time of the last edition of this HTM, in 1980, have been either withdrawn or radically revised. Some of them, in turn, are now being replaced by European Standards which will be published during the currency of this edition of HTM 2010. Some
of these European Standards support new European Union Directives on medical devices which will have a major impact on sterilization. Where practicable the information in this HTM has been aligned with existing or anticipated standards and advice is offered where no standard has yet been formulated.

The sterilizers described in this HTM may not be suitable, without modification, for safely processing articles infected with Hazard Group 4 pathogens nor agents, such as those associated with transmissible spongiform encephalopathies, which are unusually resistant to sterilization. Design considerations for sterilizers intended to process articles infected with such organisms are discussed in Part 2.

This part of HTM 2010 contains detailed supplementary information that expands upon the guidance given in Parts 1 to 4 and should be read in conjunction with them.

Information about Hazard Groups may be found in the HSC document ‘Classification of pathogens according to hazard and categories of containment’ (second edition 1990) compiled by the Advisory Committee on Dangerous Pathogens.
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Section A

Lethality of heat sterilization processes; the $F_o$ concept
A1.0 Introduction

A1.1 There are several, well established, time temperature relationships for thermal sterilization methods which are regarded as equally acceptable (see Part 3 of this HTM, Table 8, page 41). Clearly temperatures other than those shown, when maintained for an appropriate time, will also be capable of producing a sterile product.

A1.2 For a moist heat sterilization process, we can expect a particular time at a particular temperature to have a predictable lethal effect against a standardised population of organisms. If we choose particularly resistant organisms and assume they are present in numbers in excess of that likely to be encountered in real product we can define standard exposure conditions which will always yield a sterile product in a correctly operated sterilizer. Actual exposures can then be related to these standard exposure conditions.

For example, in the laboratory it is possible to produce conditions where the time to attain a pre-selected sterilization temperature, and the time to cool to ambient temperature after sterilization, is so short that it may be disregarded: a so-called “square wave exposure” system. This will enable very accurate determinations of the thermal resistance of micro-organisms under well defined conditions, and from several such determinations at different temperatures an accurate determination of the change in thermal resistance with temperature to be made.

Operational sterilizer cycles do not produce this rapid heating and cooling but have relatively slow temperature changes. The product is thus exposed to temperatures somewhat below the chosen sterilizing temperatures for considerable periods. It is apparent that there will be some lethal effect on micro-organisms during the heating and cooling phases of any particular sterilization cycle since microbial death occurs over a wide range of temperatures, albeit at different rates.

The $F_0$ concept recognises this and allows us to take account of the lethality obtained during the heating and cooling phases.

A1.3 For heat sensitive products it is desirable to minimise the heat treatment given to the product and reduce the energy input to a level which, while providing adequate assurance of sterility, will minimise the degradation of the product. Because the $F_0$ concept allows us to take account of the inactivation of micro-organisms throughout the cycle, not just during the sterilization hold period, we can thus obtain a cycle with the required lethality but with minimum thermal degradation.

A1.4 In summary, optimisation of thermal sterilization processes may be achieved by means of the $F$ method which uses a knowledge of the lethality of the particular process at different temperatures to assess the overall lethality of the cycle and express this as the equivalent exposure time at a specified temperature.

A1.5 $F$ is defined as the equivalent time in minutes at 121.1°C to produce a given sterilization effect.

A1.6 Where the specified temperature is 121.1°C (250°F) and the Z value is 10°C the term $F_0$ is used.
The $F_0$ value of a saturated steam sterilization process is the lethality expressed in terms of the equivalent time in minutes at a temperature of 121ºC delivered by that process to the product in its final container with reference to microorganisms possessing a $Z$ value of 10.

The total $F_0$ value of a process takes account of the heating up and cooling down phases of the cycle and can be calculated by integration of lethal rates with respect to time at discrete intervals.

A1.7 The $F_0$ method may be used for assessment, or control, of processes where difference in temperature is the only factor influencing the efficacy of the cycle. For example, it may be applied to the steam sterilization of aqueous fluids in sealed containers but it is not applicable to steam sterilization of porous loads where air removal is also a key factor and failure to achieve direct contact with Dry Saturated Steam can lead to failure, regardless of whether the required temperature was achieved within the load.

A1.8 Similar concepts are also used for dry heat sterilization processes and for depyrogenation by exposure to dry heat.

A1.9 There are a number of pre-requisites which it is necessary to consider before the use of the $F_0$ method is appropriate. These include:

- the efficacy of the sterilization process under consideration is dependent only on temperature eg air removal is not critical. Thus in a porous-load steam sterilizer where impaired air removal can allow air to persist in random locations throughout the load, and where it may be present in sufficient quantity to impair sterilization, the use of the $F_0$ method for cycle control or monitoring is inappropriate;
- the sterilizer to be used has cycle control which is adequate to ensure that production cycles consistently reproduce the conditions established during validation. $F_0$ monitoring of a process may not be used to justify the use of a sterilizer which demonstrates excessive temperature variation within the load or poor reproducibility from cycle to cycle etc;
- temperature profile studies/validation studies have been conducted to establish the uniformity of conditions throughout load and to identify the location of those parts of the load which are slowest to heat up and fastest to cool down;
- the loading composition and pattern of production cycles is controlled within the limits established during validation to ensure that the results obtained remain valid;
- production controls and bioburden studies are adequate to maintain a known, low level, of microbial contamination and the thermal resistance and temperature dependence ($D$ and $Z$ values respectively) of the most resistant contaminant(s) are known or the assumed values are in accordance with the Pharmacopoeial recommendations.
A2.0 Fundamental concepts

A2.1 In order to use the $F_0$ concept correctly it is important to understand the facts, definitions and assumptions on which the model is based. It has become common place to use certain functions and terms in the analysis and interpretation of data on the effect of physical or chemical stress on microbial survival. These terms are discussed below.

How microbes die: the logarithmic order of death

A2.2 Organisms which die as a result of an imposed stress die in an orderly, and predictable, manner. This can be represented as survivor curve, showing the number of organisms still living at various times after the beginning of exposure to the stress condition.

A2.3 The order of death is, in principle, the same for all multicellular organisms. The survivor curve remains constant for as long as individuals can recover from that length of exposure; then as the first individuals die, the frequency of death rapidly increases until only a few very resistant organisms remain, and they succumb shortly after the majority of the population (see Figure A1). In a unicellular organism the individual is dead when a single cell dies, whereas in multicellular organisms the death of one cell is not likely to kill the Individual. The multicellular organism will survive until enough cells have been killed to cause death.

![Figure A1](image)

Figure A1 Arithmetic survivor curve for multicellular organisms

A2.4 Whichever multicellular organisms are tested, for example insects or plants, and whatever the lethal stress, the survivor curve remains essentially the same. This was accepted as universally true for all organisms until the early 1900s when workers such as Harriet Chick [see Chick (1908)] showed that in an homogeneous culture of a single strain of bacteria the cells died at a constant rate when exposed to a particular lethal stress.
A2.5 It was apparent that these bacteria were dying in a manner which was somewhat unexpected. This may be illustrated by taking as an example the survival of microbial spores subjected to heat stress. An experiment may be devised in which all factors other than the heating time are held as constant as possible. If a number of biological indicators, each bearing a known number of bacterial spores, are subjected to a thermal sterilization process, at a predetermined temperature for various increments of exposure time, and then the survivors on each indicator enumerated, the data obtained shows the number of colony forming units remaining viable after each exposure time.

A2.6 A survivor graph can be prepared showing the number of survivors as a function of the length of heating time. Both the number of survivors and the time may be plotted on an arithmetic scale (see Figure A2).

Unicellular bacteria

![Arithmetic survivor curve for unicellular bacteria](image)

A2.7 Alternatively the number of survivors may be plotted on a logarithmic scale as a function of time on the arithmetic scale, which is referred to as a semi-log survivor curve (see Figures A3 and A4). While both the arithmetic and semi-log survivor curves accurately represent the death of bacteria the latter is more useful in sterilization studies where interest is concentrated on the rate of destruction as the number of survivors approaches zero.

Multicellular organisms

![Semi-log survivor curve for multicellular organisms](image)
A2.8  It is usual to use the latter approach since in sterilization studies we are interested in the rate of destruction as the number of surviving micro-organisms approaches zero, which is best shown using a logarithmic plot.

Unicellular bacteria

Figure A4 Semi-log survivor curve for unicellular bacteria

A2.9  Experience has shown that the semi-log survivor curve for heat stress often approximates to a straight line for part or all of the survivor curve. However there are many recorded instances where deviations from the “ideal” straight line condition occur (see Figure A5).

Figure A5 Microbial survivor curves showing typical deviations from the linear model; curve a is a theoretical linear survivor curve; curve b shows an initial “shoulder” followed by a linear survivor curve; curve c shows an initial increase in count, “activation”, followed by a linear survivor curve; curve d shows an initial linear survivor curve followed by a decreasing rate of kill, “tailing”; curve e shows the sigmoidal survivor curve often encountered in experimental determinations.
Conditions resulting in a non-logarithmic order of death

A2.10 Typical survivor curves for bacterial spores exposed to moist heat sterilization processes are shown in Figure A5 in which the logarithm of the number of surviving organisms is plotted against time and various types of response are illustrated:

- **Curve a** - exponential - constant fraction of the population is inactivated per unit time;
- **Curve b** - shows an increasing death rate after an initial period where there was little or no inactivation - a “shoulder”;
- **Curve c** - initial activation (increase in population) followed by a constant death rate;
- **Curve d** - decreasing death rate with a low number of highly resistant organisms surviving for a prolonged period - “tailing”;
- **Curve e** - a sigmoidal survivor curve of the type frequently encountered in experimental determinations of resistance. This type of survivor curve may be regarded as a composite of elements of the survivor curves described above.

Factors influencing the nature of the survivor curve

A2.11 There are a number of factors which have a significant effect on the nature of the survivor curve. Workers such as Moats et al. (1971) have discussed these factors in detail. Some of the key factors can be summarised as follows:

- **Growth index.** During recovery there are many instances when not all viable spores will germinate and outgrow within a short time period. The percentage of those present which do germinate and grow immediately on incubation is referred to as the growth index. The growth index varies both with the species of bacterial spore and the cultural conditions in which it was grown and is to be recovered. It may be as high as 100%, for example for Bacillus subtilis, but may be as low as <1%, for example for Bacillus stearothermophilus. Sublethal heating may increase (activate) or decrease (deactivate) the growth index and give rise to non-linear survivor curves. [see Favero (1967), Finley and Fields (1967)] The interaction of activation and inactivation on the thermal treatment of heat resistant dormant spores of B stearothermophilus can be described mathematically. [see Shull et al. (1963)]

- **Cell clusters.** The usual method of counting the number of surviving bacteria is by the plate count method which gives the number of colonies developed from a known volume of suspension inoculated onto the surface of solid growth medium. The number of colonies is equal to the number of bacteria present only when each colony arises from a single cell.

When the cells are in clusters, for example Staphylococcus spp., or in chains, for example Streptococcus spp., one colony may represent a large number of cells. All the time there are one or more surviving cells within the aggregation a colony will be formed and death therefore becomes evident only when the last cell is dead. Such clusters “die” like multicellular organisms and show convex survivor curves (see Figures A3 and A5, curve b).
Cell age. It has been demonstrated that young cells, that is, the exponential growth phase of a culture, are more susceptible to both chemical and physical stress than old cells from the stationary phase of a culture. Furthermore if old cells are transferred to a new environment they do not all begin to grow at the same time and a culture develops in which both old and young cells coexist leading to heterogeneous resistance and concave survivor curves (see Figure A5, curve d).

Mixed populations. Where more than one strain or species is present, with different resistances to the lethal stress being imposed, a non-linear survivor curve, typically of concave form, will arise (see Figure A5, curve d).

Factors influencing the heat resistance of spores

A2.12 Any assessment of thermal resistance of micro-organisms must involve consideration of those factors which may affect the thermal resistance.

A2.13 These factors include the species and strain of organisms to be considered; its physiological state, which will in part depend on its immediate cultural history, the manner in which it is presented to the sterilization process, for example the suspending menstruum; and the recovery conditions which are used in an attempt to grow the organism after exposure to the process; as well as the exposure conditions used, for example whether dry heat or moist heat (direct contact with dry saturated steam or being in an aqueous solution) was used, and the exposure temperature. [see Russell (1971)]

A2.14 The nature of the product also affects the thermal resistance of contaminating organisms; the protective effects of various salts and carbohydrates in solution are well documented in the literature.

A2.15 The influence of changes in the manufacturing environment and/or process on the nature and extent of contaminating micro-organisms must also be considered.

Treatment of sterilization-process microbial survival data

A2.16 A mathematical approach to the resistance of bacteria to thermal death is required to allow calculation of equivalent lethality. Two factors need to be considered; the thermal resistance of the micro-organism at a particular temperature and the change in that resistance which occurs with changes in temperature.

These two factors are analogous to the rate constant and temperature coefficient of a chemical reaction, respectively.

A2.17 Spore inactivation in moist heat may be considered as a monomolecular first order reaction, that is where the rate of reaction is governed by the concentration of the reactant, in this case the bacterial spores.
This may be expressed as

\[
\frac{dN_a}{dt} = k \cdot C_a
\]

where \( t \) = time,
\( C_a \) = spore concentration
\( k \) = a reaction rate constant at constant temperature

Then \( \left( \log C_a \right)_t - \left( \log C_a \right)_0 = k \left( t - t_0 \right) \)

where the superscript 0 indicates initial conditions

**A2.18** A semi-logarithmic plot of concentration versus time will yield a straight line of slope \( k \). \( k \) has dimensions of time\(^{-1}\). The negative reciprocal of the rate constant \( k \) is equivalent to the number of minutes required to inactivate 90% of the organisms present, that is a 1 log reduction. This value is referred to as the \( D \) value and, as stated, mathematically it is inversely proportional to the inactivation rate constant \( k \)

\[
D = \frac{2.303}{k}
\]

**Decimal reduction value (D value)**

**A2.19** The \( D \) value is used as a measure of the resistance of a defined micro-organism to a defined sterilization process. It is a convenient way to describe the slope of a linear semi-log survivor curve.

**A2.20** More particularly it may be defined as the extent of exposure, under stated conditions, necessary to produce a 90%, or 1 log, reduction in the bacterial population (see Figure A6). It is usually stated in minutes, except for sterilization processes using ionising irradiation where it is given in kiloGreys (units of absorbed radiation dose).

![Figure A6 Decimal reduction value](image-url)
For moist heat sterilization processes it is often given a subscript to indicate the temperature at which it was determined, for example $D_{121}$. Although this in itself is insufficient definition of the conditions under which the determination was made to allow valid comparison.

The $D$ value is only relevant to the survivor curve when the survivor curve is truly a straight line over the range of population values of interest, including the “probability” zone.

It is not necessary to construct a survivor curve to determine $D$ value. The determination may be done by a replicate unit method involving fractional-unit-negative (FN) data. A number of replicates are heated for a certain time and the number viable and the number sterile are determined. [see Pflug and Schmidt (1968)]

$$N_U = \log(n(r/q)) = 2.303 \log (r/q)$$

and

$$D = \frac{\text{duration of treatment (min)}}{\log \text{ initial no} - \log \text{ final no of spores}} = \frac{U}{\log N_0 - \log N_U}.$$  

The temperature dependence of resistance

A common measure of the temperature dependence of a chemical reaction is the $Q_{10}$ value. This is defined as the change in reaction rate constant $k$ for a 10°C change in temperature:

$$Q = \frac{k(T+10^\circ\text{C})}{k_T}.$$  

For most chemical reactions $Q_{10}$ has a value of about 2, but for spore inactivation in moist heat $Q_{10} = 10$ to 18 and for spore inactivation in dry heat $Q_{10} = 2.2$ to 4.6.

Other measures of temperature dependence include the Arrhenius equation;

$$k = A \exp \left(-\frac{E_A}{RT}\right)$$

where $k$ = the reaction rate constant; $A$ = the frequency factor; $E_A$ = the activation energy; $R$ = the universal gas constant; $T$ = the absolute temperature.
However, the temperature dependence of reaction rates for spores is generally expressed as a Z value,

$$ Z = \frac{\log Q_{10}}{10} $$

or

$$ Z = 2.303 \frac{RT}{E_A^2} $$

**Z value**

The Z value is a measure of the change of inactivation rate with temperature. It is the slope of a plot of D value on a logarithmic scale against temperature on an arithmetic scale (see Figure A7).

The Z value allows comparison of the lethal effect of heating at different temperatures. [see Bigelow (1921)]

As originally defined Z is numerically equal to the number of degrees Fahrenheit change in temperature required to reduce the D value by 90%, or 1 log. Considerable confusion, and error, can be caused where the temperature scale used is not specified. Although values are now usually given in °C care must be taken when using published data, for example from the official compendia, to note whether the D value is quoted in °F or °C.

The mathematical relationship with the D value can be expressed as:

$$ \log D_2 - \log D_1 = \frac{(T_1 - T_2)}{Z} $$

It should be noted that, the greater the Z value, the greater the increase in temperature which is required to give a tenfold decrease in D value. Hence the assumption of a Z value higher than in fact exists will give an additional margin of safety. The Z value assumed for most thermophiles, such as *Bacillus stearothermophilus*, is 10°C.
The straight-line relationship holds good only over a limited temperature range for an homogenous culture of a single strain of microorganisms. Mixed cultures give a non-linear relationship, but in practice one sub-population, either by virtue of its resistance or its prevalence, will be controlling with regard to attainment of sterility.

**Lethal rates**

The usefulness of the temperature dependent model lies in being able to calculate the lethality over a range of temperatures, which will include those experienced during heating-up and cooling-down of a load in a steam sterilizer.

The relative lethality at a temperature $T_{\text{exp}}$, compared to the known lethality at a particular reference temperature $T_{\text{ref}}$, is dependent on the Z value.

Thus, the lethality $L$ is given by the equation

$$L = 10^{\frac{T_{\text{ref}} - T_{\text{exp}}}{Z}}$$

Lethality factors for any temperature deviation from the reference temperature and for any Z value can be calculated using this formula (see Table A1).

A new variable $F$, the thermal death time can be defined. The change in $F$ with temperature is analogous to the change in thermal resistance ($D$ value) with temperature and both are dependent on the Z value. Plots of log $D$ versus temperature and log $F$ versus temperature both have slope $Z$:

$$\frac{D_{T}}{D_{121}} = \frac{F_{T}}{F_{121}} = 10^{\frac{T - 121}{Z}}$$

**$F$ value**

The $F$ value expresses heat treatment in terms of the equivalent effect of a stated time at some stated temperature for a particular Z value, that is to say that the $F$ value is the equivalent time in minutes at $121.1^\circ C$ ($250^\circ F$) for an organism of specified Z value.

$F_0$ is the $F$ value when $Z$ is $18^\circ F$ ($10^\circ C$):

$$F_0 = \sum 10^{\frac{T - 121}{Z}} t$$

where $t$ is the chosen time interval, and $T$ is the temperature in the container.

**Note** For dry heat $F$ values, $F$ is equal to the time in minutes at $176^\circ C$ ($350^\circ F$).
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Lethality \( L \) is given by:

\[
L = 10^{\frac{T_{ref} - T}{Z}} - 1
\]

* Lethality factor is given in minutes equivalent at the reference temperature
A3.0 Sterility

A3.1 In order to utilise the $F_0$ method it is first necessary to decide on the extent of treatment which will be necessary to provide the required level of assurance that the product is sterile. Several different definitions are in common use.

Sterility assurance

A3.2 If the survivor curve is extrapolated beyond log$_{10} 0$, that is one surviving organism, we reach a region of “probability” of finding a single surviving organism. For example at log$_{10} [-1]$ we expect to find, not 0.1 organisms surviving in every sample but, one in every ten samples with a surviving micro-organism.

We can thus determine from the survivor curve a theoretical probability of any one unit of product being non-sterile.

A3.3 The European standard, EN556, in common with a definition in the European Pharmacopoeia, states that a product may be regarded as sterile when the theoretical level of not more than one micro-organism is present in $1 \times 10^6$ sterilized units of the final product.

A3.4 This calculation may be based on data, obtained by investigation, on the extent and resistance of microbial contamination immediately prior to sterilization (the Bioburden) or on a theoretical contamination of $10^6$ micro-organisms per unit of product presumed to be of a type having known high resistance to the process, for example bacterial spores. In the latter case the cycle is often referred to as a “12D” or “overkill” cycle and was first proposed by Esty and Meyer (1922) for processing low-acid canned food products.

A3.5 The British Pharmacopoeia in Appendix XVIII ‘Methods of Sterilization’ states: “For aqueous preparations sterilized by heating in an autoclave the preferred combination of temperature and time is a minimum of 121ºC maintained throughout the load during a holding period of 15 minutes.” However, it goes on to say: “Other combinations of time and temperature may be used provided that the process chosen delivers an adequate level of lethality when operated routinely within the established tolerances.”

A3.6 In Annex 2, ‘Guidance on application of the $F_0$ concept to aqueous preparations.’ the British Pharmacopoeia suggests that “In general for aqueous preparations a microbiologically validated steam sterilization process that delivers, in total, an $F_0$ value of not less than 8 to every container in the load is considered satisfactory.”

A3.7 In certain circumstances, however, use of a steam sterilization process that delivers, in total, an $F_0$ of less than 8 may be considered justifiable, for example where the product is especially heat sensitive. The nature of processes delivering an $F_0$ of less than 8 is such that great care must be taken in order to ensure that adequate assurance of sterility is consistently achieved. It is necessary not only to validate the process microbiologically but also to perform continuous, rigorous microbiological monitoring during routine production to demonstrate that the microbiological parameters are within established
tolerances so as to give a theoretical level of not more than one living micro-
organism per 10^6 containers in the final product.

A3.8 The European Pharmacopoeia also states that the recommended method
for parenteral products is moist heat sterilization at a minimum of 121°C
maintained throughout the load for a minimum of 15 minutes. Other time
temperatures can be used but the crucial requirement is delivery of an
adequate level of “lethality” to the product. The use of F_0 is recognised with an
F_0 of 8 being the usually acceptable minimum. It is emphasised that this
requires a low pre-sterilization bioburden and the absence of heat resistant
spores.

Calculation of F_0 values

A3.9 Reliable F_0 value calculations are simply achieved with modern
microprocessor based control and monitoring systems. However F_0 values can
be calculated manually, and many of the available computer programs employ
essentially similar methods:

a. **Graphical method.** In the graphical method F reference paper is used on
which the lethal rate per minute, at particular temperature, is represented
by length on the vertical axis. The horizontal axis has a corresponding
arithmetic scale for time such that the area of a rectangle delineated by
the ordinate 121.1°C and a length corresponding to one minute on the
abscissa is equal, by definition to an F_0 of one. The cumulative area under
the curve as the cycle progresses represents the cumulative lethality of the
process (see Figure A8). In practice the temperature profile is plotted and
the area under the curve determined using a planimeter. The area
measured is then converted to an F_0 value using the scale of the F
reference paper.

b. **Summation method.** In the summation method the lethal rate at each
specific temperature is calculated or read from a table (see Table A1) and
multiplied by the time for which that temperature persisted. The values
obtained for each temperature are summed to give the overall F_0 value
for the cycle.

A3.10 The accuracy of the integration is affected by a number of factors.
These include:

- the choice of time interval between successive temperature
  measurements. BS 3970 Part 2 specifies a maximum interval of two
  seconds;
- whether the minimum, maximum or average temperature during the
  chosen time interval is used. (Since the method is an approximation based
  on summing discrete data to represent continuous data there will always
  be some error, which may be positive or negative; each may be correct
  for different purposes);
- the location of the sensor(s) from which the temperature is read and the
  adequacy of the validation of sensor location;
- should be used only over the temperature range for which Z has been
determined. The Z value for any micro-organism does not remain
constant over all possible temperatures. Therefore any particular lower
temperature limits for the integration need not be set since, for a Z value
of 10, F_0 values below 105°C make so little contribution. For example, 40
minutes exposure at 105°C is equivalent to one minute at 121°C.
Figure A8  Graphical determination of $F_0$ values. The ordinate scale (temperature) of
$F$-reference paper is proportional to the lethal rate so that the area beneath
the curve is a measure of the $F$ value. The cumulative values during the
cooling stage are not used for sterilizer control but may be used in monitoring
to provide an accurate assessment of the overall lethality delivered by the
sterilization cycle. Within each box the figures in italics indicate the $F_0$ value
calculated for that time-temperature rectangle. The lower figures indicate
the cumulative $F_0$ value through the cycle. The $F_0$ controller, set to provide an
$F_0$ value of 9, initiates the cooling stage at point A. The total monitored $F_0$
value of the cycle is 11.99.
A4.0 Applications of the $F_0$ concept

**General**

A4.1 Part 3 of this HTM states that if a fluid sterilizer is fitted with an $F_i$ integrating system, then the recorder should be capable of computing and printing values of $F_0$ for each channel with integration times no greater than 2 s. This is also a requirement of BS 3970: Part 2.

**Control of sterile cooling fluid (in a steam sterilizer for fluids in sealed containers)**

A4.2 It is a requirement that if the coolant is derived from a water or steam service and is intended to come into contact with the load containers, the operating cycle must expose the coolant to sufficient heat to ensure that it is free of microbial contamination by the end of the holding time. This is checked by calculating an $F_i$ value for the heat treatment received by the coolant. If the test recorder is not capable of calculating $F_i$ both BS 3970 and Part 3 of this HTM recommend the following procedure:

a. from the measured temperatures, identify the point during the heat-up time at which the coolant temperature first reaches 108°C. Note the temperature (T°C) at subsequent one minute intervals until the end of the holding time;

b. for each measurement, calculate the incremental $F_i$ ($\Delta F_i$) from the following equation:

$$\Delta F_i = \log_{10} \left[ \frac{T - 121}{10} \right] \text{ minutes}$$

where $T$ is the lowest temperature of the coolant water for each one minute time interval

c. the $F_0$ value is the sum of all $\Delta F_i$.

The test should be considered satisfactory if the $F_0$ for the coolant is not less than 8 minutes.

**$F_i$ controlled sterilizers - Control of operating cycles in steam sterilizers for fluids in sealed containers**

A4.3 The operating cycle for steam sterilizers used to process aqueous fluids in sealed containers may be divided into several stages.

1. heat up (and, where necessary, air removal) - the chamber atmosphere attains the required temperature;
2. equilibration time - all parts of the load attain or exceed the minimum temperature of the sterilization temperature band;
3. holding time - all parts of the load are maintained at a temperature within the sterilization temperature band;

4. cooling stage - the load is cooled to a temperature at which it will be safe to handle.

**A4.4** Stages 2 and 3 may be controlled by one of the following:

a. adjustable timers of an automatic controller in conjunction with temperature sensors within the active chamber discharge and within containers of the load;

b. a simulator control system;

c. an $F_0$ system.

**A4.5** Provision for adjustment of the equilibration time (stage 2) is necessary and may be achieved by one of the following:

a. an operator adjustable timer on the instrument panel;

b. a simulator control system;

c. an $F_0$ integrating system.

**A4.6** When an $F_0$ control system is fitted, the control function should be limited to the initiation of the cooling stage (stage 4) once a selected $F_0$ value has been attained.

**A4.7** In addition to the minimum requirement of two temperature sensors (see 13.1.4 of BS 3970 Part 1) two further temperature sensors shall be provided for use in two load containers.

**A4.8** The control system shall be designed to integrate from the temperatures sensed within containers of the load at selected locations at time intervals not exceeding 2 seconds.

**A4.9** The range of $F_0$ values selectable shall include 1 to 30.

**A4.10** When tested in accordance with Test method 1, the individual values of $F_0$ determined using the reference instrument shall be within the ranges stated in Table A2 for each of the $F_0$ values indicated by the sterilizer under test.

**Monitoring operating cycles in steam sterilizers for fluids in sealed containers**

**A4.11** For aqueous products in sealed containers temperatures are measured (with thermocouples or RTDs) throughout the heating and cooling stages as well as during the sterilization hold period. The slowest container to heat and the fastest container to cool may be used to determine the minimum lethality received by the load. These locations are often found in different locations.

**A4.12** Determination of the maximum temperatures in the load may also be necessary for thermolabile products where deterioration may be a problem.

---

<table>
<thead>
<tr>
<th>Table A2</th>
<th>Permitted ranges for $F_0$ values</th>
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<tr>
<td>$F_0$ value indicated by sterilizer under test</td>
<td>Permitted range for $F_0$ values determination by the reference instrument*</td>
</tr>
<tr>
<td>1</td>
<td>1 to 105</td>
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<tr>
<td>15</td>
<td>15 to 15.7</td>
</tr>
<tr>
<td>30</td>
<td>30 to 31.5</td>
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</table>

* The reference instrument is described in Test method 2.
A4.13 It is essential that during commissioning and validation it is established that the position of containers which need to be monitored remains consistent from cycle to cycle. A sterilizer where the slowest part of the load to reach temperature is found in different parts of the load on successive cycles is not suitable for control or monitoring by $F_0$ values and is in urgent need of skilled attention. For air-ballasted sterilizers this may involve additional requirements on monitoring the circulation of the chamber atmosphere to ensure that the location of the cool point remains constant.

A4.14 Calculation of the $F_0$ value delivered by a process may be estimated from the lowest temperature-time curve registered from the containers in the load. The process is satisfactory if the registered $F_0$ value is within the minimum and maximum limits established during validation.

Validation of operating cycles in steam sterilizers for fluids in sealed containers

A4.15 The use of $F_0$ control or monitoring systems places additional requirements on the validation process.

A4.16 As described in Part 3 of this HTM, paragraph 8.4 ‘Sterilizer function using a full load’ ‘... the temperature of all sites monitored within the load ...... shall be within 1°C of each other throughout stage 3’. This requirement applies regardless of whether an $F_0$ system is used.

Container cool point

A4.17 Container mapping is necessary to determine the container cool point. Container mapping studies should be conducted prior to conducting loaded chamber heat penetration studies in order to determine the position within the liquid-filled container which is slowest to attain temperature.

A4.18 Small volume containers and those of cylindrical form where the length:diameter ratio is large are the least likely to demonstrate a detectable cold spot.

The number of thermocouples within the container should be sufficient to monitor the upper, middle and lower layers of the central region of the container. Using an excessive number of temperature probes may introduce significant errors in the determination.

A4.19 The profile point requiring the longest exposure time to equilibrate with the chamber temperature should then be used in subsequent $F_0$ studies and monitoring (but see later for degradation/product stability considerations).

A4.20 Suitable container entry systems for the insertion of temperature probes into sealed containers are described in part 3 of this HTM (Figure 3, p 40)

A4.21 Independent measuring equipment should be to the standard described in part 3 of this HTM, Chapter 6.
**A4.22** The test should be carried out as described in part 3 of this HTM for a thermometric test for a full load (see paragraph 14.10) except that the load should be containers of the type and number to be used in practice and filled with the product to be sterilized or a suitable substitute with similar thermal characteristics. (see paragraph A4.31 below).

**Load cool point**

**A4.23** It is necessary to determine the coolest point within a specified load type and configuration of load. Cool points arise because of varied rate of heat transfer throughout the load and studies are needed to ensure that the cool points are identified so that they may be exposed to sufficient heat lethality.

**A4.24** The study is carried out in the same manner as the performance qualification described in part 3 of this HTM (see paragraphs 8.13 to 8.28 performance qualification, pp 57 to 59)

**A4.25** Similar studies may be used to identify those containers which attain temperature maxima or most prolonged exposure to the equilibrium temperature for product degradation and/or stability studies.

**A4.26** The $F_0$ value for the process may then be determined by integrating the lethal rates throughout the heating process using one of the methods previously described.

**Microbial challenge studies**

(See also part 3 of this HTM paragraphs 8.29 to 8.36, pp 59 - 60)

**A4.27** Biological challenges may be used during validation studies in order to demonstrate the process lethality provided by the sterilization cycle. Calibrated biological indicators used for this purpose act as bioburden models and can be used in obtaining data to calculate $F_0$ values delivered by the cycle or to supplement physical temperature measurement, for example from thermocouples.

**A4.28** The number of spores to be used in the BI can be calculated from the following formula

\[
D_{\text{prod}} (\log N_{\text{prod}} + 6) = D_{\text{bi}} (\log N_{\text{bi}} + 1)
\]

where 
$D_{\text{prod}}$ = the resistance of the most resistant organisms in the product bioburden;
$N_{\text{prod}}$ = the number of organisms in the product to be sterilized;
$D_{\text{bi}}$ = the resistance of the BI organisms;
$N_{\text{bi}}$ = the number of organisms on the BI.

**A4.29** Designated liquid-filled containers are inoculated with the indicator organism by injecting an aliquot of a calibrated spore suspension into the suspending menstruum to provide the calculated concentration of spores. The containers chosen should be those previously established by temperature measurement as having the lowest delivered lethality.

**A4.30** The suspending menstruum should be the product to be sterilized unless this contains preservatives, antimicrobials or other substances which inhibit the growth of the indicator micro-organisms.
A4.31 If it is necessary to use a product substitute it should be selected to have similar physical characteristics to the product this should include heat capacity (specific heat), density, viscosity, thermal conductivity.

A4.32 Great care needed when using inoculated product to minimise the possibility of contaminating the production environment.

A4.33 Microbial challenge studies should be conducted concurrently with heat penetration studies.

**Product degradation and stability versus cycle lethality**

A4.34 When heat-sensitive thermolabile products are to be sterilized it is important that adequate assurance of sterility is not obtained at the expense of product degradation or stability.

A4.35 For sterilization the temperature dependence of the process is described by the Z value, that is the change in temperature required to give a tenfold change in the rate of microbial kill. Increasing or decreasing the temperature of the process requires a corresponding decrease or increase in exposure time to maintain the same cycle lethality or $F_0$ value.

A4.36 For any given temperature, microbial death and chemical degradation take place at different rates. The relationship between time and temperature which exists for microbial lethality cannot be extrapolated to the product degradation reaction.

A4.37 If the degradation reaction is not altered significantly by the change in temperature the extent of degradation will increase as process (exposure) time is extended. Conversely, if the degradation reaction is highly temperature dependent (high activation energy) a decrease in temperature may more than compensate for the increase in time, resulting in less degradation.

A4.38 The key variable is the activation energy, $E_a$. If the activation energy for the chemical degradation reaction is lower than that of the microbial death curve, that is it is less temperature dependent, then it can be assumed that a decrease in sterilization temperature will result in greater product degradation.

A4.39 Furthermore it cannot be assumed that sterilization cycles of equivalent lethality, but which differ with regard to time and temperature, will yield product of equal quality.

A4.40 The assumption that degradation reactions follow first-order reaction kinetics is probably a good approximation in most cases where a single active drug product is contained in the solution.

A4.41 Experience has shown that a decrease in sterilization temperature can have a marked deleterious effect on product and its long term stability.

A4.42 Sterilization of glucose solutions in plastic containers may require a sterilization temperature in the range 115-118°C in order to protect the thermolabile container. The increased time required for sterilization compared with a traditional cycle at 121°C used for similar solutions in glass bottles results in a noticeable increase in caramelization.
A4.43 The activation energy of the lethal reaction for bacterial spores with a 
Z value of 10°C is high (typically around 60 kcal/mole) compared to most first-
order liquid-phase decompositions. Thus products that degrade with heat are 
more affected by an increase in time than an increase in temperature. For 
example, expressed as a Z value the temperature effect of the degradation of 
glucose would have a Z value of about 33°C.

A4.44 The use of F values based on the Z value of the most resistant 
contaminating organism found during bioburden studies rather than an 
assumed Z value of 10°C may be necessary for particularly thermolabile 
products. Great care is needed in the application of this technique because of 
the inherent variability of microbial contamination and the rigorous process 
control and monitoring needed to minimise this.

Product stability

A4.45 Product stability may also be related to degradation during 
sterilization. Chemical reaction kinetic studies on many products indicate that 
product stability over the desired shelf life can be extrapolated from the extent 
of degradation measured just after sterilization. In some cases a degradation 
product formed during sterilization triggers subsequent deterioration and the 
specific factors affecting the formation of the degradation product would need 
to be investigated.

A4.46 Both microbial lethality and degradation are cumulative with respect to 
time and temperature, so variations in the heating and cooling phases of the 
cycle will affect the extent of degradation, and thus product stability, as well as 
lethality.

A4.47 Degradation and stability studies should consider the entire cycle and 
not just the dwell time. These effects are more pronounced for products where 
the degradation reaction has a lower activation energy.

A4.48 F values are generally calculated from the coolest part of the load. For 
degradation and stability purposes the hottest part of the load is of more 
consequence. The entire range of temperature and time experienced 
throughout the load must be recorded in order to substantiate degradation and 
stability claims.

Cycle development studies

A4.49 Determination of F values is often of value in the development of 
appropriate operating cycles for steam sterilization of both fluids in sealed 
containers and wrapped goods and porous loads. However, since temperature 
measurement alone cannot reliably detect failure to obtain direct contact with 
dry saturated steam, it is not practicable to use F values for monitoring or 
controlling porous load cycles.

The use of F values for porous load cycles should be limited to determining 
suitable sublethal cycles for biological challenge studies.
A5.0 Test methods

Test for $F_0$ control compliance

Apparatus
A5.1 Glass bottle, of nominal capacity 1 litre, complying with DIN 58363.
A5.2 Independent $F_0$ reference instrument, as described in section F.

Procedure
A5.3 Install the reference instrument.
A5.4 Place 1 litre of cold water in the bottle. Insert the two temperature sensors of the $F_0$ control system and the sensor of the reference instrument so that the sensing points of all three are at about 85% of the bottle depth and over the approximate centre of the bottom of the bottle. Seal the bottle.
A5.5 Select the required $F_0$ value on the control panel and perform a cycle in which automatic control is terminated manually immediately at the beginning of stage 4. Note the value of $F_0$ shown by the reference instrument.
A5.6 Repeat the procedure described in paragraph A5.5 twice.
A5.7 This test procedure shall be carried out for $F_0$ values of 1, 15 and 30.
A5.8 Calculate the mean of the three replicate values for each setting of $F_0$ control and check for compliance with the values given in Table A2.

Test for performance of reference instrument

Apparatus
A5.9 Temperature regulated heat source capable of being controlled at a given temperature within 0.10°C in the range 115°C to 126°C.
A5.10 Thermometer traceable to national standards to include the range 100°C to 130°C complying with BS 593 and graduated at intervals of 0.1°C.
A5.11 Temperature logging device computing $F_0$ values of the sensor(s) with integration at least every 2 s and means of print out, together with suitable temperature sensor(s).
A5.12 Stopwatch.

Procedure
A5.13 Install the sensor(s) into the temperature regulated heat source.
A5.14 Adjust the heat source so that it maintains a temperature of 121±0.1°C.
A5.15 Allow the equipment to integrate $F_0$ for 15 minutes timed with the stopwatch. Note the indicated $F_0$ value.

A5.16 Repeat with the temperature source maintained at $115\pm0.1^\circ\text{C}$ for 30 min.

A5.17 Repeat with the temperature source maintained at $126\pm0.1^\circ\text{C}$ for 10 min.

A5.18 The replicate $F_0$ values obtained at $121^\circ\text{C}$ shall lie within the range 14.66 to 15.34.

A5.19 The replicate $F_0$ values obtained at $115^\circ\text{C}$ shall lie within the range 7.36 to 7.71.

A5.20 The replicate $F_0$ values obtained at $126^\circ\text{C}$ shall lie within the range 30.90 to 33.36.
Glossary

**D value**
The *D* value (or Decimal Reduction Value) is a measure of the resistance of a micro-organism to a particular type of sterilization process. It is the value of the appropriate parameter of the process (duration or absorbed dose) required to reduce the number of viable micro-organisms to 10% of the original number.

In connection with sterilization by heating in an autoclave the *D* value is expressed by the time in minutes at a defined temperature (the temperature is often shown as a subscript, for example $D_{121.1}$).

**Z value**
In connection with sterilization by heating in an autoclave the *Z* value relates the heat resistance of a micro-organism to changes in temperature. The *Z* value is the change in temperature required to alter the *D* value by a factor of 10.

**$F$**
A quantity, measured in minutes, used to determine the efficacy of an operating cycle and equivalent to a continuous period at a temperature of 121.1°C for an organism with a *Z* value of 10°C.
Bibliography


Section B

Methods for determining the fatigue life of rectangular pressure vessels
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B.0 Methods for determining the fatigue life of rectangular pressure vessels

The section which follows contains Appendix C of BS3970, reproduced with permission of the British Standards Institute.

Appendix C. Design of pressure vessels with rectangular section

C.1 General

This appendix specifies requirements for the design of welded pressure vessels of rectangular cross section and of all connections, supports, brackets or other attachments (directly welded or attached by some other means) to the pressure-containing shell.

The maximum design stress shall comply with section two of BS 5500 : 1988 for category 2 vessels and shall comply with 3.4.2 of BS 5500 : 1988 for category 3 vessels.

For vessels constructed from copper, appendix B of this Part of BS 3970 shall apply.

C.2 Fatigue loads

C.2.1 The minimum thickness of material for the vessel shall be determined for each operating cycle (see C.4.2).

NOTE. For further guidance, see clause 3 of BS 5500 : 1988.

C.2.2 In the design of the vessel, account shall be taken of all fluctuating stresses which the vessel is intended to withstand during its service life. Consideration shall be given to (but is not limited to) the following possible sources of cyclic or repeated stresses:

(a) periodic temperature transients;
(b) restriction of expansion or contraction during normal temperature variation;
(c) application or fluctuations of pressure and/or temperature;
(d) forced vibration;
(e) variations in external loads.

NOTE. Fatigue failure is frequently associated with the presence of a 'notch', which may be a score mark, or a discontinuity such as a change in cross section, more or less abrupt, with transition sections of different curvatures. Alternatively, notches may be the attachment for supports or penetrations into the shell in the form of drilled holes or welded nozzles with varying diameters and corner radii. As these features give rise to local concentrations of stress, they are to be taken into consideration, together with bending stresses arising from eccentricities of load path, because these stresses can significantly effect the fatigue life of the vessel.

C.2.3 Provision shall be made in the design to permit thermal expansion and contraction so as to avoid excessive stress during the expected changes in temperature.

C.2.4 Consideration shall be given to the fatigue processes that are accelerated in certain environments. Special consideration shall be given to the following (see also 3.3 of BS 5500 : 1988).

(a) Crevice corrosion. An estimate shall be made of the maximum rate of crevice corrosion and time to grow to a size which is regarded as unacceptable.

NOTE. Crevices include cracks, lack of fusion or penetration, pores, pits and re-entrant corners that are exposed to a corrosive or erosive environment.

(b) Corrosion fatigue. If the vessel is to be subjected to a particularly aggressive environment, it shall be demonstrated by reference to previous experience or specific tests, that the fatigue stresses can be tolerated for the required lifetime of the vessel and the weldments.

C.3 Stress analysis

C.3.1 General

C.3.1.1 The equations given in this clause shall be used for the calculation of membrane and bending stresses developed in vessels of the types illustrated in figures 2 to 5. The maximum total stress at a given location shall be taken to be the sum of the membrane stress and the peak bending stress at that location. The longitudinal corners of the vessel shall have a radius not less than three times the wall thickness. It is permissible for the end closure or back plate of the vessel not to be radiused to the main vessel.

C.3.1.2 For the purposes of C.3.2 to C.3.8, inclusive, and of C.4, the following symbols apply.

\[ a \] inside corner radius of sterilizer vessel (in mm)
\[ a_1 \] inside corner radius of sterilizer jacket (in mm)
\[ A \] cross-sectional area of reinforcing member attached to short side of vessel (in \( \text{mm}^2 \))
\[ A_1 \] cross-sectional area of reinforcing member attached to long side of vessel (in \( \text{mm}^2 \))
\[ b \] unsupported width of flat plate between reinforcing elements (in mm)
\[ b_c \] pitch between centrelines of door reinforcing members (in mm)
\begin{align*}
b_l & \text{ pitch between locks/latches securing door (in mm)} \\
b_s & \text{ pitch between centrelines of reinforcing members on vessel (in mm)} \\
b_i & \text{ maximum pitch between stays measured either horizontally or vertically (in mm)} \\
c & \text{ distance from neutral axis of section to outer fibre of section (in mm)} \\
C & \text{ a constant} \\
d & \text{ diameter of hole or width of slot in jacket plate for welding of stay (in mm)} \\
d_i & \text{ distance between jacket plate and vessel wall (in mm)} \\
E & \text{ Young's modulus of elasticity (in N/mm}^2) \\
f & \text{ maximum allowable design stress for material (in N/mm}^2) \\
F & \text{ peak stress arising from a local discontinuity (in N/mm}^2) \\
G & \text{ distance across closure of vessel between location of gasket load reaction (in mm)} \\
h & \text{ inside length of long side of sterilizer vessel (in mm)} \\
h_i & \text{ distance between neutral axes of reinforcing members on short sides of sterilizer vessel (in mm)} \\
h_s & \text{ offset distance from gasket load reaction to bolt/latch securing vessel closure (in mm)} \\
H & \text{ inside length of short side of sterilizer vessel (in mm)} \\
H_i & \text{ distance between neutral axes of reinforcing members on long sides of sterilizer vessel (in mm)} \\
H_p & \text{ total hydrostatic end force on the vessel closure (in N)} \\
\Delta H_p & \text{ range of hydrostatic end force on the vessel closure due to pressure cycling (in N)} \\
I & \text{ second moment of area of strip of thickness \( t \) (in mm}^4) \\
I_{11} & \text{ second moment of area of combined reinforcing member and associated plate of thickness \( t \) on short side of vessel (in mm}^4) \\
I_{11} & \text{ second moment of area of combined reinforcing member and associated plate of thickness \( t \) on long side of vessel (in mm}^4) \\
I_s & \text{ second moment of area per unit length for jacketed vessel (in mm}^4) \\
I_s & \text{ second moment of area of combined reinforcing member and associated plate of thickness \( t \) for vessel closure (in mm}^4) \\
k & \text{ equivalent number of maximum stress cycles in one duty cycle} \\
K_r & \text{ factor for unreinforced sterilizer vessel to figure 2 (in mm}^3) \\
K_r & \text{ factor for reinforced sterilizer vessel to figure 4 (in mm}^3) \\
l_i, l_s, L, L_s & \text{ dimensions of the vessel (e.g. figure 4) (in mm)} \\
m & \text{ exponent in fatigue crack growth law} \\
M_e & \text{ bending moment at middle of long side; positive when outside of vessel is put into compression (in N-mm)} \\
\Delta n & \text{ total number of design stress cycles for which the vessel is to be designed (\( n > n_n \))} \\
n_s & \text{ number of stress cycles having a range \( \sigma_{r,n} \)} \\
n_n & \text{ number of stress cycles having a range \( \sigma_{r,n} \)} \\
n & \text{ total number of bolts/latches securing vessel closure} \\
N & \text{ number of stress cycles to cause failure in fatigue} \\
\rho & \text{ maximum design pressure (in N/mm}^2) \\
\Delta P & \text{ total pressure range during a pressure cycle (in N/mm}^2) \\
P_s & \text{ total allowable working load on weld (in N)} \\
Q & \text{ self-equilibrating secondary stress due to thermal effects (in N/mm}^2) \\
S_b & \text{ bending stress (in N/mm}^2) \\
S_m & \text{ membrane stress (in N/mm}^2) \\
t & \text{ plate thickness of the vessel (in mm)} \\
t_s & \text{ plate thickness of the vessel closure (in mm)} \\
t & \text{ plate thickness of the jacket (in mm)} \\
W & \text{ design strength of latch securing door closure (in N)} \\
\Delta W & \text{ fatigue load range on latch (in N)} \\
\delta & \text{ maximum deflections calculated according to beam formula (in mm)} \\
\sigma_{r,1}, \sigma_{r,2}, \sigma_{r,3}, \sigma_{r,4}, \sigma_{r,n} & \text{ stress ranges (in N/mm}^2) \\
\theta & \text{ angular measure} \\
\alpha & \text{ \( H/h \)} \\
\alpha_1 & \text{ \( H/l \)} \\
\alpha_2 & \text{ \( L/l \)} \\
\phi & \text{ \( a/l \)} \\
C.3.2 Unreinforced vessels complying with figure 2} 

C.3.2.1 For unreinforced vessels complying with figure 2, the membrane stresses \((S_m)\) shall be determined from the following equations.

At \( C \),

\[(S_m)_{C} = \frac{b \theta + L}{t}
\]

At \( D \),

\[(S_m)_{D} = (S_m)_{C}
\]
At B,
\[ (S_m)_B = \frac{p}{t} \left[ (a + l_1) + \sqrt{(a^2 + l_1^2)} \right] \]

At A,
\[ (S_m)_A = (S_m)_B \]  
At the corner,
\[ (S_m)_{B-C} = \frac{p}{t} \left[ a + \sqrt{a^2 + l_1^2} \right] \]

C.3.2.2 The bending stresses shall be determined from the following equations.

At C,
\[ (S_m)_C = \pm \frac{r}{4t} \left[ 2M_A + p(2aL - 2aL_1 + L^2) \right] \]

At D,
\[ (S_m)_D = \pm \frac{r}{4t} \left[ 2M_A + p(2aL - 2aL_1 + L^2 - l_1^2) \right] \]

At A,
\[ (S_m)_A = \pm \frac{M_A t}{2l_1} \]

At B,
\[ (S_m)_B = \pm \frac{r}{4t} \left[ 2M_A + pL^2 \right] \]

At the corner,
\[ (S_m)_{B-C} = \frac{r}{4l_1} \left[ \frac{1}{2} \left( 2M_A + p(2aL \cos - l_1^2) \right) \right] \]

For these equations the following shall apply:
(a) The maximum value of \( (S_m)_{B-C} \) is given where
\[ \tan^{-1} \left( \frac{d}{l_1} \right) \]
(b) The bending moment \( M_A = \frac{pK_3}{L} \) per unit length, where:
\[ K_3 = \frac{-l_1^2 (6\phi^2 \alpha_2 - 3 \pi \phi^2 + 6 \phi^2 \alpha_3 + 3 \alpha_2^2)}{3 (2\alpha_3 + \pi \phi + 2)} \]

C.3.3 Reinforced vessels complying with figure 3

C.3.3.1 On reinforced vessels complying with figure 3, the reinforcement shall be by a continuous frame which may follow the contour of the vessel or may form a closed rectangle. The reinforcing members shall be welded to the outside of the vessel in a plane perpendicular to the long axis of the vessel. The reinforcement on two opposite sides of the vessel shall have the same second moment of area.

NOTE. The reinforcing members and the attached plate elements of the vessel are considered to act as a composite unit when calculating the effective second moment of area of the reinforcing members. If the reinforcement is not welded directly to the wall of the vessel in the corner region, the effective second moment of area at the corner is taken to be that of the reinforcement alone.

C.3.3.2 The maximum distance, \( b_R \), between the centre-lines of reinforcing members shall be not greater than 40t.

C.3.3.3 The longitudinal bending stress developed on the unsupported flat plate elements of the vessel wall between the reinforcing elements shall be determined from the equation:
\[ S_b = 0.5p \left[ \frac{b}{t} \right]^2 \]

C.3.3.4 The width, \( b \), of the unsupported flat plates between the reinforcing elements shall not exceed:
\[ b = \left[ \frac{h^2 t^2 b_{NC}}{6t_{11}} \right]^{1/2} \]

C.3.3.5 The membrane stresses shall be determined from the following equations.

For the short sides
\[ (S_m)_D = \frac{pH_B}{2(A_1 + \theta_{RT})} \]

For the long sides
\[ (S_m)_A = \frac{pH_B}{2(A_2 + \theta_{RT})} \]
C.3.3.6 The bending stresses shall be determined from the following equations:

At A,
\[ (S_{bl})_A = \frac{-pbRh^2c}{24I_{1s}} \left( \frac{2(1 + a_1^2k)}{(1 + k)} \right) \]

At B,
\[ (S_{bl})_B = \frac{pbRh^2c}{12I_{1s}} \left( \frac{(1 + a_1^2k)}{(1 + k)} \right) \]

At C,
\[ (S_{bl})_C = \frac{pbRh^2c}{12I_{1s}} \left( \frac{(1 + a_1^2k)}{(1 + k)} \right) \]

At D,
\[ (S_{bl})_D = \frac{pbRh^2c}{24I_{1s}} \left( \frac{3a^2 - 2(1 + a_1^2k)}{(1 + k)} \right) \]

For these equations the following shall apply:

(a) \( a = \frac{H}{h} \)
(b) \( a_1 = \frac{H_1}{h_1} \); and
(c) \( k = \frac{l_2l_1H_1}{l_1l_1H_1} \)

C.3.4 Partially reinforced vessels complying with figure 4
C.3.4.1 On partially reinforced vessels complying with figure 4, the reinforcement shall not be continuous around the vessel but provide only partial reinforcement of the flat surface to which it is welded.

NOTE. In practice, the reinforcement required can be expected to extend across most of the flat surface.

C.3.4.2 The membrane stresses, which for this type of vessel are based only on plate thickness, shall be determined from the following equations.

For short sides,
\[ (S_{m})_A = \frac{ph}{2t} \]

For long sides,
\[ (S_{m})_A = \frac{ph}{2t} \left( \sqrt{L^2 + l_1^2} \right) \]

At the corner,
\[ (S_{m})_{C-D} = \frac{p}{t} \left( a + \sqrt{L^2 + l_1^2} \right) \]

For these equations the following shall apply:

(a) \( \frac{r}{h} \geq \left( \frac{3p}{t} \right) \left( \frac{1 - 2L}{H} \right) \)
(b) \( \frac{r}{H} \geq \left( \frac{3p}{f} \right) \left( \frac{1 - 2L}{H} \right) \)

Figure 3. Reinforced vessels

Figure 4. Partially reinforced vessels
C.3.4.3 The bending stresses shall be determined from the following equations.

At A,
\[
[S_b]_A = \frac{cM_A}{I_{11}}
\]

At B,
\[
[S_b]_B = \frac{c}{I_1} \left[ M_A + \frac{\rho L^2 \theta_R}{2} \right]
\]

At C,
\[
[S_b]_C = \frac{c}{I_1} \left[ M_A + \frac{\rho L^2 \theta_R}{2} \right]
\]

At D,
\[
[S_b]_D = \frac{c}{I_1} \left[ M_A + \frac{P \theta_R}{2} \left( \frac{L}{2} + a(L - l_1) \right) \right]
\]

At E,
\[
[S_b]_E = \frac{c}{I_1} \left[ M_A + \frac{P \theta_R}{2} \left( \frac{L}{2} + 2a(L - l_1) - l_i \right) \right]
\]

At F,
\[
[S_b]_F = \frac{c}{I_1} \left[ M_A + \frac{P \theta_R}{2} \left( \frac{L}{2} + 2a(L - l_1) - l_i \right) \right]
\]

At the corner,
\[
[S_b]_{C-D} = \frac{c}{I_1} \left[ M_A + \frac{P \theta_R}{2} \left( \frac{L}{2} + aL \cos \theta - aL_i (1 - \sin \theta) \right) \right]
\]

For these equations the following shall apply:
(a) the maximum value of \([S_b]_C = D\) is given where \(\theta = \tan^{-1}(L/L_1)\) vertical, and
(b) the bending moment \(M_A = \rho \theta_R K_4\), where:
\[
K_4 = -12L^3 - L_1^3 - L_2^3 - 2L_{12}^3 + 12aL^3 + 3\pi aL^2 - 12aL^3 + 12aL (L_i - L_2) + 6L^2 (L_i - L_1) + 12aL^3 + 6aL^3 - 6aL^3 \pi + 12aL^3 +
-2L_3 \frac{L_1}{L_3} + \frac{2L_1}{L_3} \frac{L^3}{L_3} \frac{L^3}{L_3} + 3L^2 L_2 -
-3L_2 \frac{L_1}{L_2} + 6aL^2 \frac{L_2}{L_2} + 6aL^2 \frac{L_2}{L_2} \]
\[= \frac{6}{L_2} \left( 2L_2 - L_1 - L_2 + \pi \frac{\pi}{d} \right) \]
\[
[S_b]_{C-D} = \frac{c}{I_1} \left[ M_A + \frac{P \theta_R}{2} \left( \frac{L}{2} + aL \cos \theta - aL_i (1 - \sin \theta) \right) \right]
\]

C.3.5 Jacketed vessels complying with figure 5

C.3.5.1 The jacket, if fitted, shall be an integral pressure chamber attached to the main sterilizer vessel by welded stays. The welds attaching the stays to the vessel shall terminate not less than \(\frac{d}{2}\) from the commencement of the curvature of the corners indicated as points B and C of the jacket.

C.3.5.2 The maximum bending stress, \(S_b\), on the welds attaching the stays to the jacket plates shall be determined from the equation:
\[
S_b = C_{пл} \left[ \frac{h_3}{d} \right]^{2.5}
\]
where:
\(C = 4\) for fillet and partial penetration welds;
\(C = 3\) for full penetration welds;
\(d\) shall be not less than \(2t_3\).

NOTE. The bending stress range produced by pressure cycling should be used to determine the fatigue life of these welds.
C.3.5.3 The peak design bending stress, $S_b$, for the plates of the main vessel and jacket shall be determined from the following equations.

NOTE. Bending stresses at the corners B and C are negligible.

At A

$$S_{bA} = \frac{cM_A}{l_i}$$

At D

$$S_{bD} = \frac{cM_D}{l_i}$$

For these equations the following shall apply:

- $c$ is measured to the inside surface of the vessel.

C.3.5.4 The maximum membrane stresses shall be determined from the following equations.

At A,

$$S_{mA} = \frac{\rho (L + a)^2}{2}$$

At B,

$$S_{mB} = \frac{\rho a + \sqrt{(L^2 + l_i^2)}}{t + t_i}$$

At C,

$$S_{mC} = S_{mA}$$

At U,

$$S_{mD} = \frac{\rho (L + a)}{t + t_i}$$

C.3.6 Structure surrounding door openings

The maximum deflection, normal to the plate, of the vessel wall around the door opening shall not exceed 0.05$L$. If the reinforcing is considered to be fully built-in at the corners of the vessel, then the maximum deflection, $\delta$, shall be determined from the equation:

$$\delta = \frac{p0 (L + a)^2}{96E l_i}$$

but, if the reinforcing at the door surrounds is simply supported at the corners of the vessel, the above deflection shall be increased by a factor of 5 (see note 1).

NOTE 1. It may be necessary to reinforce the vessel locally around the door openings to meet requirements for stiffness in this region.

NOTE 2. The reinforcing structure around the door opening may also provide for the redistribution, into the walls of the vessel, of the loads arising from the door locks and latches. The forces carried by the individual locks and latches are transmitted to the vessel walls and result in local forces and moments being applied to the vessel walls. Significant peak stresses can develop locally giving a reduced fatigue life. Care should be taken to minimize offsets in load paths between the vessel wall and the latch loads, otherwise significant bending stresses may be introduced into the vessel wall. An analysis of the peak stresses occurring in this region should be performed and an assessment of the fatigue life made in accordance with C.4.

C.3.7 Reinforced door structure

C.3.7.1 Reinforcing members shall be welded to the outside of the door in a plane parallel to either the long or short sides of the door.

NOTE 1. A door with horizontal reinforcing members is illustrated in figure 7.

Each of the reinforcing members shall have the same second moment of area. The distance, $b_{OD}$, between the centrelines of reinforcing members shall be not greater than $40t_D$.

NOTE 2. The reinforcing and the attached plate elements of the door are considered to act as a composite unit when calculating the effective second moment of area of the reinforcing members.

NOTE 3. Additional reinforcing may be necessary around the edge of the door to reduce deflection in the area of the seals.

C.3.7.2 The latches shall be designed to withstand the operating conditions of the hydrostatic end force exerted by the design pressure on the area bounded by the line of gasket load reaction and to maintain sufficient compressive force on the gasket to ensure a tight seal.

NOTE. In general latches and bolting will be pre-loaded to give improved fatigue life and ensure closure of the joint between the vessel and the door.

C.3.7.3 The maximum deflection on any part of the door, relative to points where the latches react against the pressure force, shall be not greater than 0.1$L$. For a door reinforced as illustrated in figure 7, the maximum deflection occurring at the centre of the door reinforcement shall be determined from the equation:

$$\delta = \frac{G^2}{16E l_D}$$

C.3.7.4 The maximum bending stress occurring at the centre of the door due to pressure loading and latch loads shall be determined from the equation:

$$S_{bD} = \frac{p_bD G^2}{2\pi} \left(1 + \frac{\pi h_G}{G}\right)$$

where the value of $W$ is zero for doors continuously supported along the edge and is not less than $2H_b/h_L$ for clamped doors.

C.3.7.5 For fatigue analysis, the cyclic bending stress shall be determined from the equation:

$$\sigma_c = \frac{c}{l_D} \left[\frac{\Delta p_bD G^2}{2\pi} \left(1 + \frac{\pi h_G}{G}\right)\right]$$
C.3.7.6 The latches securing the door shall be designed for a fatigue loading given by the equation:

\[ \Delta W = \Delta H_p / (n_L - 2) \]

The bending stress developed in the unsupported flat plate between reinforcing elements shall be determined from the equation:

\[ S_b = 0.5p \left( \frac{b}{t_D} \right)^2 \]

C.3.8 Door locks and latches, hinges and mechanisms

C.3.8.1 Devices used to secure the door and react against the pressure force acting on the door, back into the walls of the vessel shall operate on at least two opposite sides of the door.
C.4 Fatigue assessment

C.4.1 General

C.4.1.1 Each part of a constructional detail which is subjected to fluctuating stress shall have a particular class designated in accordance with the criteria given in table 4, in which the figures illustrate the geometrical features and potential crack locations.

Details not covered in table 4 shall be treated as class G, or class W for load-carrying weld metal, or shall be proved by special fatigue tests.

NOTE. Such test data should be sufficiently extensive to allow the d vs. N or the δ vs. N safe design curves to be determined for the material, geometry and loading of the design detail under consideration.

C.4.1.2 The life of the vessel shall be determined on the basis of an operating cycle in which the maximum pressure and temperature variations are those to be used during the lifetime of the vessel.

C.4.1.3 The total number, no. of design stress cycles for which the vessel is to be designed shall be determined from the equation:

\[ n_a = 2k_1 n \]

where

\[ k_1 \]

has the value determined from the equation:

\[ k_1 = \left[ 1 + \frac{1}{\frac{\sigma_{12}}{\sigma_{11}}} \right]^3 + m_1 \left[ \frac{1}{\frac{\sigma_{12}}{\sigma_{11}}} \right]^3 + m_2 \left[ \frac{1}{\frac{\sigma_{12}}{\sigma_{11}}} \right]^3 \]

or 1.5, whichever is the greater;

\[ \delta_{12} \]

is the stress range resulting from the maximum pressure differential in the duty cycle;

\[ \delta_{11} \]

is the next most significant stress range resulting from the largest pressure change in any part of the duty cycle;

\[ \delta_{12}, \delta_{11} \]

are the stress ranges resulting from each range of pressure variations in the duty cycle.

C.4.1.4 The relevant stress used for fatigue analysis shall be the cyclic stress range, which is the sum of the cyclic components of membrane (S_m), bending (S_b), thermal (Q) and discontinuity (F) stresses. If the design load spectrum consists of variable amplitudes of these stress intensities, then the maximum values of these variables shall be used for the analysis.

C.4.2 Particular design features

C.4.2.1 Consideration shall be given to the appropriate stress to be used in the fatigue assessment dependent upon the design detail and the likely crack initiation sites and propagation paths.

C.4.2.2 For parent material and full penetration butt welds, the cracks initiating from weld toes, fastener holes, faying surfaces and propagating through parent material or fully penetrated weld metal shall be assessed using the nominal principal stress range in the member at that point.

NOTE. Local stress concentration effects of a weld profile, a fastener hole, etc. should be ignored as these are taken into account in the (stress cycles) data for the appropriate class or category of design detail. However other larger geometrical effects which may give rise to concentrations of stress and secondary bending stresses should be taken into account. The presence of residual stresses may be ignored for welded joints as these are already included in the (stress cycles) data.

C.4.2.3 For fillet and partial penetration butt welds, the cracks initiating from weld roots and propagating through the weld throat shall be assessed using the vector sum of the shear stress in the weld metal based on an effective throat dimension.

C.4.2.4 For threaded fasteners under axial load, the cracks initiating at thread roots shall be assessed using the mean axial stress on the core area of the fastener.

NOTE. If bending is also present, the peak stress should be used calculated on the flexural rigidity of the core.

C.4.3 Design procedure

C.4.3.1 Determine the joint classification of each weld detail in accordance with table 4.

NOTE. The classifications may be deemed to include, for the effects of any accidental misalignment up to the lesser of 0.15 X Y thickness of the thinner part or 3 mm, provided that the root sides of joints with single-sided preparations, i.e. single bevel -J, -U or -V forms, are back-gouged to a total width at least equal to half the thickness of the thinner element.

C.4.3.2 Calculate the maximum stress range arising at each weld detail from the peak sterilization cycle of vacuum to maximum working pressure.

C.4.3.3 Determine from the fatigue design curves shown in figures 8 and 9 the number of cycles to failure, N, due to the stress range calculated in C.4.3.2, using the Young's modulus of elasticity, E, of the material for the design temperature of the vessel.

C.4.3.4 Check that the number of cycles N determined in C.4.3.3 is greater than 2 k_1 n.

C.4.3.5 If the number of cycles to failure N, determined in C.4.3.3 is less than the number of design cycles in C.4.3.4, strengthen the weld detail to reduce the value of δ,E. Alternatively, redesign the detail to a higher class.
<table>
<thead>
<tr>
<th>Classification</th>
<th>Design detail</th>
<th>Description</th>
<th>Notes</th>
</tr>
</thead>
<tbody>
<tr>
<td>E</td>
<td></td>
<td>Bolted joint</td>
<td>Class E applies to fatigue assessment of joints fastened by precision bolts in close tolerance holes and secured by lock nuts torqued to full capacity. It also applies to the assessment of an attachment at the location of an intermediate gap in a long weld running in the direction of loading but away from the weld end. At full penetration, transverse welds join two simple plates end to end. Thickness and width variation (less than 1 in 4 in slope) and surface misalignments may be included. Any undercut should be ground smooth.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermediate gap in a long weld</td>
<td></td>
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<tr>
<td></td>
<td></td>
<td>Transverse butt weld</td>
<td></td>
</tr>
<tr>
<td>F</td>
<td></td>
<td>Continuous fillet weld with narrow attachment</td>
<td>Class F applies to fatigue assessment at a long, fillet welded, narrow attachment, whose width is less than 50 mm. It includes short transverse welds less than 160 mm long in a direction normal to the loading. It also applies to the transverse full penetration butt welds on a permanent backing strip or where there is a third member transverse through joint. If the third member is a plate with continuity plating, allowing the main member stress to be continued through the transverse member without offset, the stress on net area is used. If there is no continuity plating, the stress used should be the peak stress concentration at the joint. Where two flat plates intersect in the same plane, as in the case of flanges, a stress concentration factor of four due to the abrupt change of width should be used.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Transverse fillet welded cover plate</td>
<td></td>
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<tr>
<td></td>
<td></td>
<td>Transverse butt weld with backing strip</td>
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<td></td>
<td>Full penetration cruciform butt weld</td>
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</tr>
<tr>
<td>Classification</td>
<td>Design detail</td>
<td>Description</td>
<td>Notes</td>
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<tr>
<td>F2</td>
<td></td>
<td>Fillet welded attachment</td>
<td>Class F2 applies to fatigue assessment: (a) at an attachment weld, where the weld is longer than 150 mm in the direction of the loading and the attachment is less than 50 mm wide; and (b) at transverse full penetration butt welds joining two simple plates end to end, where there is an abrupt change in width. It also applies: (c) at joints of rolled or extruded steel members of similar profile, where the reinforcement is dressed flush and the misalignment slope is less than 1 in 4; (d) at transverse joints where the end of one member is welded by partial penetration butt or fillet weld to the side of another member or where there is a third member transverse through partial penetration butt weld.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Full penetration butt weld, with abrupt change of width</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Partial penetration load carrying weld or load carrying fillet weld</td>
<td></td>
</tr>
<tr>
<td>G</td>
<td></td>
<td>Long welded attachment</td>
<td>Class G applies to fatigue assessment at a weld-end of long welded attachment in the direction of loading, where the attachment is greater than 50 mm wide. The length of weld parallel to the loading is assumed to be greater than 150 mm. It also applies at any attachment close to the edge of the member. In all cases care should be taken to avoid undercut on element corners. Weld returns across corners should also be avoided.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Wing butt welded attachment</td>
<td></td>
</tr>
<tr>
<td>Classification</td>
<td>Design detail</td>
<td>Description</td>
<td>Notes</td>
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</tr>
<tr>
<td>W</td>
<td></td>
<td>Root failure in weld metal for fillet or partial penetration welds</td>
<td>Class W applies to fatigue assessment of weld material transverse to the loading in any incompletely fused joint, partial penetration butt or fillet weld. The stress should be calculated on the effective weld throat area.</td>
</tr>
</tbody>
</table>
Figure 8. Design (σ, E vs. N) fatigue curves
Figure 9. Fatigue strength of steel bolts
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C1.0 Introduction

C1.1 This section discusses the factors which should be considered in the selection and use of packaging for terminally sterilized products, that is, those materials which are sterilized in their packaging.

Packaging for medical equipment which has been cleaned, decontaminated/disinfected and serviced ready for return to use is not included in this guidance.

C1.2 It does not consider those products which are sterilized and then aseptically packed in sterilized packaging materials nor does it cover packaging of terminally sterilized components to be used in aseptic manufacturing.

Sterilization processes

C1.3 Because the product is sterilized in its packaging it is necessary that the packaging material is compatible with the sterilization process to be used.

C1.4 The sterilization processes included are those which are generally available for use either directly or through a sub-contractor. It does not include requirements for new processes which are currently under development or at an early stage of their introduction for practical use. This would include, for example, those systems employing gaseous or plasma phase peracetic acid and/or hydrogen peroxide.

C1.5 Sterilization processes included are:
   a. Steam - for clinical use (see HTM 2010 Part 1, paragraph 2.1 (a)):
      (i) for wrapped goods and porous loads;
      (ii) for aqueous fluids
            " in rigid containers;
            " in flexible containers;
      (iii) for unwrapped instruments and utensils
            " externally supplied steam;
            " internally generated steam;
   b. Steam - for laboratory use (see HTM 2010 Part 1, paragraph 2.1 (b));
   c. Low-temperature steam and formaldehyde. Note. The packaging materials, systems and procedures described are also suitable for use with disinfection processes intended for use with wrapped goods, for example Low Temperature Steam Disinfectors (LTS);
   d. Ethylene oxide
   e. Dry heat (hot air)
   f. Ionising irradiation (gamma and beta)
Product applications

C1.6 The sterile products for which packaging is considered include:

- medical devices and surgical instruments:
  - primarily those products, including re-useable instruments, utensils and textiles, which are processed by Sterile Service Departments, including units directly serving operating theatres (although the same principles apply to other manufacturing systems which have a wide range of product specifications produced singly or in small numbers. Only passing reference is made to high speed automated packaging systems.);
  - re-useable instruments processed in clinics and general practices (dental and medical);
- pharmaceutical manufacturing of sterile products;
- laboratory product manufacturing, for example culture media for microbiology;
- discard (or make-safe) prior to disposal of potentially infective material.

C1.7 Consideration is given to materials and systems for both single-use and re-usable packaging.

C1.8 Single-use packaging includes, for example, ampoules, single-trip bottles, paper bags, paper/plastic pouches & reels, paper wraps, vacuum formed trays, etc.

C1.9 Re-usable packaging includes, for example, multiple-trip bottles, procedure trays, sterilization containers, textile wraps, etc.

C1.10 This guidance section also makes reference to labelling, storage and distribution giving both guidance and particular requirements necessary to ensure compliance with extant regulations.

Responsibility

C1.11 Part 1 of HTM 2010 (paragraph 1.15 (h)) identifies the procedures for production, quality control and safety as a major responsibility of management.

C1.12 The provisions of this section should be reviewed by those responsible for the management of sterile production and adapted to local circumstances (for example taking into consideration the nature of the product, the volume of production, the sterilization process(es) available etc).

C1.13 It should be used as the basis for the development of written policies, specifications and procedures to be used in the control of sterile production.

General performance requirements

C1.14 The purposes for which packaging is used are:

- to contain the product;
- to permit sterilization of the packaged product;
- to protect the product from deterioration and damage;
• to maintain the sterility of the product through distribution and storage to the point of use;
• to prevent contamination of the product.

C1.15 In addition the packaging must:
• permit identification of the number and type of product contained, the lot number, the manufacturer and the expiry date (by labelling);
• include specification of storage conditions which the packaging is designed to withstand;
• provide any necessary instructions for the correct use of the product (by labelling and/or instruction sheets);
• present the product in a manner which allows it to be removed aseptically immediately before use.

Packaging operations

C1.16 The procedures and controls implemented for packaging operations must be designed to ensure that:
• each product produced is in the correct type of pack;
• each pack is correctly and effectively sealed;
• each pack is correctly labelled with all the necessary information.

Quality control

C1.17 The nature of packaging for terminally sterilized products is such that:
• it is not possible to test the packaging on finished product in a manner which permits its subsequent distribution for use;
• it is not possible to test any one sample for all necessary characteristics;
• it is not possible to test each pack immediately before use to ensure that the packaging has performed correctly throughout sterilization, distribution and storage.

C1.18 Adequate control of the quality of packaging can only be obtained through a comprehensive programme including:
• design, and design verification;
• specification of packaging procedures;
• validation of packaging procedures;
• control of purchased material;
• control and monitoring of the packaging process;
• training for all who produce, handle or use sterile packs.

C1.19 Labelling is an essential part of packaging and procedures are required to ensure that particular care is taken to avoid labelling errors.

C1.20 The importance of proper control over all aspects of the packaging process cannot be over-emphasised. When products such as medical devices or medicinal products are presented wrongly labelled, contaminated, or damaged their use can cause serious adverse effect and may, in extreme cases, be lethal.
C2.0 Regulatory requirements and standards

C2.1 So far as requirements for packaging, including labelling, are concerned, the chief areas of legislation with which managers should be familiar are those concerned with safety, consumer protection, medicinal products, medical devices, active implantable medical devices and in vitro diagnostics.

The legislation relevant to sterilizers is also discussed in HTM 2010 Part 1, Chapter 3, to which reference should be made.

Safety

C2.2 Manufacturers have two specific obligations under the Health and Safety at Work etc. Act 1974:

a. to take all reasonably practicable steps to ensure that their products have been designed and manufactured so as to be safe when used for the intended purpose;

b. to ensure that persons who use their product in further manufacturing and retailing operations have adequate information and advice about how the products should be used to ensure safety.

C2.3 There is also a more general requirement under common law to protect all persons involved with the use of the product.

Medicinal products

C2.4 Where a packaging material or system is used to contain a medicinal product the licensing provisions of the Medicines Act 1968 apply.

Further information may be found in ‘Guidance to the NHS on the licensing requirements of the Medicines Act 1968’ published by the Medicines Control Agency.


Guide to Good Manufacturing Practice for medicinal products

C2.6 The principles and detailed guidelines of good manufacturing practice deal with a number of aspects of packaging including:

- Documentation, which should include:
  - a formal, written specification for packaging materials;
  - formally authorised packaging instructions for each product, pack size and type;
  - a record kept for each batch or part batch processed.
• Purchase, handling and control should be treated in the same manner as starting materials with particular attention paid to printed material;

• Packaging operations should be designed to minimise the risk of mix-ups by the inclusion of a line clearance procedure and special care should be exercised to avoid mislabelling.

The packaging should be verified as being of the correct type, clean and in the correct quantity and there should be suitable on-line control and monitoring to verify the adequacy of the packaging operation.

**Consumer protection**

**C2.7** Part 1 of the Consumer Protection Act 1987 implements Directive 85/374/EEC (the Product Liability Directive) and provides for compensation to be paid to persons suffering injury from a defective product. The implications of this legislation are discussed in HTM 2010 Part 1 (paragraphs 3.26 to 3.28 inclusive).

**Active Implantable Medical Device Regulations 1992**

**C2.8** The Active Implantable Medical Devices Regulations 1992 (Sl/1992/3146) implements Council Directive 90/385/EEC. Schedule 2, paragraph 7 of these regulations requires active implantable medical devices to be designed, manufactured and packed in a non-reusable packaging according to procedures which are sufficient to ensure that:

a. the device is sterile when placed on the market;

b. if handled in accordance with conditions as to storage laid down by the manufacturer, the device remains sterile until the packaging is removed and the device is implanted.

**Medical Devices Regulations**


**C2.10** Regulation 11 concerns the procedure for systems and procedure packs and requires, inter alia, that any person who puts devices bearing the CE marking together, within their intended purpose and within the limits of use specified by their manufacturers, in order to place them on the market as a system or procedure pack, shall draw up a declaration by which he states that he has packaged the system or procedure pack and supplied relevant information to users incorporating relevant instructions from the manufacturers, and that the whole activity is subjected to appropriate methods of internal control and inspection.

**C2.11** The Essential Requirements described in Annex 1 (of the Directive) include a number of specific requirements for packaging and labelling which are summarised below.
General requirements

C2.12 The devices must be designed, manufactured and packaged in such a way that they are suitable for the functions specified by the manufacturer.

C2.13 The devices must be designed, manufactured and packed in such a way that their characteristics and performances during their intended use will not be adversely affected during transport and storage taking account of the instructions and information supplied by the manufacturer.

Requirements regarding design and construction

C2.14 The devices be designed, manufactured and packed in such a way as to minimise the risk posed by contaminants and residues to the persons involved in the transport, storage and use of the devices and to the patients taking into account the intended purpose of the product.

C2.15 The devices and manufacturing processes must be designed in such a way as to eliminate or reduce as far as possible the risk of infection to the patient, user and third parties.

C2.16 Devices delivered in a sterile state must be designed, manufactured and packed in a non-reusable pack and/or according to appropriate procedures to ensure that they are sterile when placed on the market and remain sterile under the storage and transport conditions laid down, until the protective packaging is damaged or opened.

C2.17 Packaging systems for non-sterile devices must keep the product without deterioration at the level of cleanliness stipulated and, if the devices are to be sterilized prior to use, minimise the risk of microbial contamination; the packaging system must be suitable taking account of the method of sterilization specified by the manufacturer.

C2.18 The packaging and/or label of the device must distinguish between identical or similar products sold in both sterile and non-sterile condition.

C2.19 Each device must be accompanied by the information needed to use it safely and to identify the manufacturer, taking into account the training and knowledge of the users.

C2.20 This information comprises the data on the label and the data in the instructions for use.

C2.21 As far as practicable and appropriate, the information needed to use the device safely must be set out on the device itself and/or on the packaging for each unit or, where appropriate, on the sales packaging.

C2.22 If individual packaging of each unit is not practicable the information must be set out in the leaflet supplied with one or more devices.

C2.23 Instructions for use must be included in the packaging for every device. By way of exception, no such instructions for use are needed for devices classified in Class I or IIa if they can be used safely without any such instructions. The majority of, but not all, products produced in hospital based sterilization units would fall into this category, for example re-usable surgical instruments which are in Class I. Exceptions include implants, and may include devices intended for use on skin wounds that have breached the dermis. In case of doubt reference should be made to the classification criteria given in
Annex IX of the directive or advice sought from the competent authority (Medical Devices Agency, DoH).

C2.24 Where appropriate is information should take the form of symbols. Any symbol or identification colour used must conform to the harmonised standards. In areas for which no standards exist, the symbols and colours must be described in the documentation supplied with the device.

C2.25 The label must bear the following particulars:
   a. the name and trade address of the manufacturer;
   b. the details strictly necessary for the user to identify the device and the contents of the packaging;
   c. where appropriate, the word STERILE;
   d. where appropriate, the batch code, preceded by the word LOT, or the serial number;
   e. where appropriate, an indication of the date by which the device should be used, in safety, expressed as the year and month;
   f. where appropriate, an indication that the device is for single use;
   g. if the device is custom made, the words “custom made device”;
   h. if the device is intended for clinical investigations, the words “exclusively for clinical investigations”;
   i. any special storage and/or handling conditions;
   j. any special operating instructions;
   k. any warnings and/or precautions to take;
   l. year of manufacture for active devices other than those covered by e. This indication may be included in the batch or serial number;
   m. where applicable, method of sterilization.

C2.26 If the intended purpose of the device is not obvious to the user the manufacturer must clearly state it on the label and in the instructions for use.

C2.27 Wherever reasonable and practicable, the devices and detachable components must be identified, where appropriate in terms of batches, to allow all appropriate action to detect any potential risk posed by the devices and detachable components.

C2.28 Where appropriate the instructions for use must contain the following particulars:
   a. information to avoid certain risks in connection with implantation of the device;
   b. the necessary instructions in the event of damage to the sterile packaging and where appropriate details of appropriate methods of re-sterilization;
   c. if the device is reusable, information on the appropriate processes to allow re-use, including cleaning, disinfection, packaging and, where appropriate, the method of sterilization of the device to be re-sterilized, and any restriction on the number of re-uses.
C2.29 Where devices are supplied with the intention that they be sterilized before use, the instructions for cleaning and sterilization must be such that if correctly followed the device will still comply with the general requirements specified in Section I, Annex I of the directive.

C2.30 The instructions for use must also include details allowing the medical staff to brief the patient on any contra-indications and any precautions to be taken.

Glass containers EEC Directive 75/107

C2.31 Capacity tolerances for bottles specified as measuring containers were defined in the Directive and are summarised in Table C1.

Two methods of capacity verification were specified, the Standard deviation method and the Mean range method.

British and European standards

C2.32 The rapid development in European Standards, which are required to be adopted as national standards by all European members of the European Committee for Standardisation (CEN), is largely due to the role that such standards have in demonstrating compliance with legislation implementing European Directives.

CEN is recognised by the European Union as a competent body for the adoption of harmonised standards.

C2.33 For the purpose of the European Directives on Medical Devices and Active Implantable Medical Devices a harmonised standard is a technical specification (European standard or harmonisation, document) adopted, on a mandate from the European Commission, by CEN.

C2.34 There is a presumption of compliance to the essential requirements of the Directive for devices which are in conformity with the relevant harmonised standards the references of which have been published in the Official Journal of the European Communities.

C2.35 A number of standards are in preparation which are relevant to packaging and labelling of terminally sterilized products.

The following list is not exhaustive. The standards discussed are in various stages of preparation, those marked * are finalised and published. All EN standards are available in the UK as British Standards; there is now a dual numbering system so that EN *** will be numbered as BS EN ***.

C2.36 EN 1041 Terminology symbols and information provided with medical devices - Information supplied by the manufacturer with medical devices

This standard specifies the information to be supplied by the manufacturer of medical devices necessary to comply with the requirements of the Directive.

C2.37 EN 980 Terminology symbols and information provided with medical devices - Graphical symbols for the labelling of medical devices

<table>
<thead>
<tr>
<th>Nominal capacity C (ml)</th>
<th>Capacity tolerances as % of C in ml</th>
</tr>
</thead>
<tbody>
<tr>
<td>50 - 100</td>
<td>±3</td>
</tr>
<tr>
<td>100 - 200</td>
<td>±3</td>
</tr>
<tr>
<td>200 - 300</td>
<td>±6</td>
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<tr>
<td>300 - 500</td>
<td>±2</td>
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<tr>
<td>500 - 1000</td>
<td>±10</td>
</tr>
<tr>
<td>1000 - 5000</td>
<td>±1</td>
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</tbody>
</table>
This standard defines a number of symbols to be used in labelling medical devices. The use of these symbols will both facilitate provision of all the essential information on small packs and minimise the need for multi-lingual labelling.

C2.38 EN 868 series Packaging materials for sterilization of wrapped goods

This standard is presented in a series of separate parts. The first part specifies the general requirements for packaging materials to be used for medical devices which are to be terminally sterilized and provides requirements, guidance and test methods for the validation of packaging materials and systems.

The subsequent parts of the standard specify requirements for a variety of packaging materials and systems. Conformity with the specified requirements in these parts of the standard may be used as one means of demonstrating compliance with some, or all, of the requirements of Part 1.

C2.39 EN 867 series Non-biological systems for testing sterilizers

This series of standards specifies the requirements for chemical indicators used in testing sterilizers. Part 2 of the standard specifically addresses the performance requirements for process indicators, whether used independently of, or printed on, labels or packaging materials. Detailed specifications are given for performance criteria relevant to all the sterilization processes considered in this Section (see paragraph C1.5).

C2.40 EN 724 Guidance on the application of EN 29001 and EN 46001 and of EN 29002 and EN 46002 for non-active medical devices

This standard provides guidance on suitable methods and procedures, including aspects of packaging, for the manufacture of medical devices in conformity with the requirements of the Quality System standards which may be used to demonstrate compliance with the requirements of the Directive.

C2.41 EN 550* Sterilization of medical devices - Validation and routine control of ethylene oxide sterilization

This standard specifies requirements for the development, validation, process control and monitoring of the sterilization of medical devices using ethylene oxide and gives guidance on means by which these requirements may be met. The importance of packaging in the correct functioning of an ethylene oxide sterilization process is recognised.

C2.42 EN 552* Sterilization of medical devices - Validation and routine control of sterilization by irradiation

This standard specifies requirements for the development, validation, process control and monitoring of the sterilization of medical devices using ionising radiation and gives guidance on means by which these requirements may be met. The importance of specifying and controlling packaging from validation through to routine batch control is emphasised.

C2.43 EN 554* Sterilization of medical devices - Validation and routine control of sterilization by moist heat

This standard specifies requirements for the development, validation, process control and monitoring of the sterilization of medical devices using moist heat.
The methods used are based on monitoring physical factors and control of the packaging is an essential part of the system.

**C2.44 EN 1174 series Sterilization of medical devices - estimation of the population of micro-organisms on product**

This standard describes methods for determining the extent of microbial contamination on products, including packaging, prior to sterilization.
C3.0 Design considerations

C3.1 The manufacturer of the sterile product is responsible for adopting a design for the pack which is suitable for its intended purpose.

C3.2 However, in many cases the design of the packaging material and/or system may be controlled by the manufacturer of the packaging material and/or packaging system and sold as suitable for a particular range of applications.

C3.3 The choice of such a pre-designed, commercially available packaging system does not absolve the sterile product manufacturer from the responsibility for ensuring that:

- the design of the packaging system, including the selection of materials, is suitable in all respects for the intended application (see Chapter C6)
- the packaging system as received from the supplier is in conformity with the specification against which the choice was made (see Chapter C5)
- the production facilities, including the skills of production personnel, are compatible with the packaging system chosen and have the demonstrated capability to fill, seal and sterilize the packaging in accordance with the instructions provided by the manufacturer of the packaging system, (see Chapters C7 - C9).

C3.4 The packaging is required to fulfil a number of functions. These may be summarised as: “to minimise the safety hazard to the manufacturer, user or patient arising from interaction of the product with its environment under the conditions of sterilization, transport, storage and use as specified by the producer of the packaging system and/or sterile product.”

C3.5 The design should include consideration of at least the following:

- the compatibility of the packaging with the sterilization process;
- the compatibility of the packaging with the labelling system;
- the compatibility of the packaging with the users’ requirements at the point of use, for example aseptic opening;
- the sensitivity of the pack contents to particular risks, for example irradiation, moisture, mechanical shock, static discharge.
- the compatibility of the packaging with the contents, for example the medical device or medicinal substance, in order that the packaging has no adverse effect on the medical device or vice versa;
- the protection provided by the packaging against adverse environmental influences which may reasonably be anticipated, for example mechanical shock, vibration, chemical or microbial contamination;

C3.6 The emphasis to be given to each of these considerations will be different for each of the various sterile products manufactured but, compatibility with the sterilization process and the subsequent protection against microbial contamination are paramount in providing the user with a sterile product.
C3.7 In many cases historical data may be used to provide satisfactory evidence that the packaging is suitable for its intended purpose where packaging to the same specification has previously been used satisfactorily for a particular product, or one that is similar in all essential respects.

C3.8 The design documentation should include details of the product to be packaged, the sterilization process to be used, the storage and transport conditions as well as the specification of the packaging materials and processes to be used.

Compatibility with the sterilization process

C3.9 There are two important aspects to sterilization compatibility:

a. the ability of the packaging material to permit the attainment of the required conditions for sterilization in the process with which it is intended to be used;

b. the ability of the packaging material to withstand the sterilization process without deterioration which adversely affects its protective performance.

C3.10 Both attributes should be demonstrated.

Moist-heat/steam sterilization processes

C3.11 For effective sterilization by moist heat all parts of the load should be in contact with water or saturated steam at the required temperature for the required time.

Sterilizers for wrapped goods and porous loads

C3.12 Items to be sterilized, other than aqueous products in sealed containers, should be packaged in a pack which allows removal of air and penetration of steam but which prevents recontamination after sterilization.

C3.13 This is normally achieved by the use of materials which are permeable to air and steam but have an effective maximum pore size which is small enough to exclude microbial contamination under the specified storage and transport conditions.

C3.14 This includes wrapping in porous materials, the use of rigid containers which are fitted with filters or valves, or a combination of these methods.

C3.15 Effective sterilization requires complete permeation of the porous materials with the moisture and heat of the steam. This may occur rapidly or slowly and depends, inter alia, on the size and density of the pack, the method of air removal, the nature of the porous material etc.

C3.16 With packaged solid, hollow or fibrous products air may become trapped, randomly, in the sterilizer chamber and load. The microbial lethality of elevated temperatures under dry and moist conditions are vastly different. The presence of air can cause an unacceptable impairment of the sterilization process.

C3.17 Unpredictable air retention is of particular concern with porous wrapping materials. Hence for effective sterilization of wrapped goods and porous loads it is important to employ a sterilization process which incorporates forced air removal prior to the sterilization stage.
C3.18 Preliminary tests on the product and its packaging in order to
determine the levels and rates of change of pressure, temperature and vacuum
which start to cause unacceptable changes in the performance qualities of the
medical device and/or its packaging may be necessary.

C3.19 Performance qualification should be performed on the introduction of
new or modified packaging unless equivalence either to a validated reference
load or to previously validated packaging has been demonstrated.

C3.20 Materials used for packaging should be compatible with the
sterilization process not only in permitting passage of steam and air as required
by the process but also in not contributing any other inhibitory factors. For
example they should not generate gases which could mimic the presence of
retained air and restrict the penetration of steam.

Sterilizers for unwrapped instruments and utensils

C3.21 Sterilizers not intended for use with wrapped goods, for example bowl
and instrument sterilizers, and small transportable electrically heated sterilizers
rely on steam flow to remove air. Although the air may eventually be displaced
from wrapped loads the process is slower and less predictable than when
forced air removal is used.

C3.22 The only packaging suitable for unwrapped instrument and utensils
sterilizers are “instrument orientation” trays which are constructed of open
mesh or with sufficient ventilation holes to ensure that they present no barrier
to air removal and steam penetration.

C3.23 BS 3970 Part 4 requires that load containers for transportable sterilizers
should be designed to permit free draining of condensate and penetration of
steam by perforation of appropriate surfaces. The perforated surfaces should
have not less than 10% of their area as uniformly distributed perforations, each
perforation being at least 20 mm².

Aqueous products in sealed containers

C3.24 Sealed glass or plastics containers containing aqueous solutions permit
moist heat sterilization of the contents by virtue of the moisture present in the
product.

C3.25 The container must have a gas-tight seal if the composition of the
contents is not to be modified by evaporation of water from the contents or
the ingress and condensation of steam from the sterilizer chamber.

C3.26 The container must be able to withstand the considerable internal
pressures which will be generated during the sterilization process. This increase
in pressure arises from the volumetric expansion of the container being
insufficient to compensate for the volumetric expansion of the liquid, the
increased vapour pressure of the liquid and the increased pressure of the
heated air in the vacuity.

C3.27 The pressure generated in a correctly filled 1 litre bottle when it is
heated to 121°C may exceed 8 bar.

C3.28 Plastic containers, particularly those made of polymers which undergo
a reduction in tensile strength at the temperatures used for steam sterilization,
are often only suitable for use in sterilizers which include air or gas ballasting to
increase the pressure throughout the cycle and thus restrain the container from
bursting. A similar approach may be used to sterilized devices used as packaging, for example pre-filled syringes.

C3.29 The safety of operators will be at serious risk from the violent failure of containers and dispersal of their contents if the containers are removed from the sterilizer at too high a temperature (see HTM 2010 Part 3 paragraph 14.20 d).

C3.30 The use of unsealed containers to avoid this problem is unacceptable. Not only is the composition of the contents subject to unpredictable changes, but liquids such as molten agar might still be boiling violently. Splashes from hot liquids of high thermal capacity can cause serious burns.

C3.31 Containers which are “unsealed” but plugged with porous material, or have the cap in place but left loose, that is not screwed tightly closed, may also become unsafe at elevated temperature. The evaporation of water from residues of the contents which boiled over during the early stages of the cooling process can effectively seal the container. It is important to emphasise that these are not theoretical considerations but represent a real hazard which has, in the past, caused injury to a number of personnel.

Low-temperature steam and formaldehyde

C3.32 The basic considerations for packaging for this process are similar to those for steam sterilizers for porous loads and wrapped goods.

C3.33 However, the thermal characteristics (both the thermal capacity and thermal conductivity) of the packaging can be of importance:

a. Materials which are slow to attain the required temperature may promote the polymerisation of the formaldehyde gas.

b. Materials of high thermal capacity promote the formation of excessive quantities of condensate which also may adversely affect the sterilization process.

C3.34 In addition, the extent to which the packaging material will absorb and adsorb both moisture and formaldehyde gas may affect the efficacy of the process.

C3.35 In general packaging should be kept to the minimum compatible with adequate protection for the product and the maintenance of sterility.

Ethylene oxide

C3.36 The packaging should be designed to allow removal of air and penetration of both steam and ethylene oxide and it should be demonstrated that the specified sterilization process does not affect adversely the functioning of the packaging.

C3.37 Impervious packaging materials are unsuitable for ethylene oxide sterilization.

C3.38 There are a considerable number of different ethylene oxide sterilization processes ranging from those employing pure ethylene oxide at sub-atmospheric pressures to those which use a mixture of ethylene oxide and carbon dioxide at pressures of several bar.
C3.39 The nature of the process, including the rate of air removal and the nature of the humidification stages used, will influence the suitability of packaging to be used in the process.

C3.40 A sterilization process that employs a high moisture content and several large and rapid changes in pressure may affect the strength of package seals, with a consequent loss of integrity, whereas, package seals of the same type would have been perfectly satisfactory for a process employing less extreme conditions.

C3.41 The extent to which the packaging absorbs moisture may have a major influence on the efficacy of the process and must be considered before a satisfactory humidification stage can be demonstrated.

C3.42 The extent to which the packaging absorbs or adsorbs ethylene oxide, and its permeability to ethylene oxide may have a major influence on the efficacy of the process and the subsequent aeration process used to remove the potentially toxic residuals.

C3.43 Process control is also a concern since packaging material that has become dehydrated may absorb excessive moisture during the conditioning phase; if this possibility was not recognised during validation the achieved cycle lethality may be adversely affected.

C3.44 The use of cartons (shelf packs, transit cartons) may be convenient for handling product but increase the post-sterilization level of ethylene oxide residuals, the necessary humidification time and the length of the gas exposure stage of the cycle (by inhibiting gas penetration). All the packaging which is intended to go into the sterilizer must be compatible with the process.

C3.45 The standard on validation of ethylene oxide sterilization processes (see EN 550) includes the requirement that the packaging specification be part of the definition and documentation of the sterilization process. The validation report should include or reference details of product sterilized, including packaging specification and load patterns in the sterilizer.

C3.46 It is therefore necessary that product used for physical and microbiological performance qualification studies should be packaged in an identical manner to that to be used routinely when they are presented for sterilization.

C3.47 The introduction of a new, or altered, packaging material or system requires validation. Physical and microbiological performance qualification studies should be performed on the introduction of new or modified packaging, although demonstration of equivalence to a previously validated package would satisfy this requirement.

C3.48 Many of the packaging materials for hospital use are the same as those for use in steam sterilizers because of similar permeability requirements; however, the lower temperatures involved in the process permit a wider range of materials to be used.

Hot-air sterilizers

C3.49 The thermal conductivity, specific heat and ability to withstand temperatures of 165°C, 175°C or 185°C (depending on the process used) for extended periods, without deterioration which impairs the utility of the packaging, are obvious considerations.
C3.50 The packaging does not need to be porous since the heat transfer normally takes place by conduction.

C3.51 However, in sealed packaging the contents of the pack when heated can exert a considerable pressure and may be sufficient to rupture the packaging material or its seals.

C3.52 Vented packaging systems that allow pressure equilibration may be suitable for use in hot air sterilizers which operate with a chamber atmosphere which has been filtered through a bacteria retentive filter. This is particularly important during the post-sterilization cooling stage.

Irradiation

C3.53 The standard for validation of radiation sterilization processes (EN 552) requires that the process specification should include descriptions of the dimensions, density and orientation of the product within the packaging, as well as the pattern for the loading of product within the container to be used to transport the packs through the irradiator. This should be established and documented before commencing performance qualification studies.

C3.54 The orientation of the product during irradiation is one of the factors ensuring uniformity of dose and the ability of the packaging to maintain consistent orientation of the product must be considered.

C3.55 The density of the packaging, and hence its “transparency” to the radiation to be used may be an important consideration, particularly in the case of electron beam irradiation.

C3.56 Although radiation sterilization is a low-temperature process there is nevertheless some increase in temperature above normal ambient temperatures and this should be considered.

C3.57 There is no requirement for the packaging to be gas permeable. If the packaging is gas tight it may reasonably be assumed to be a satisfactory barrier to microbial contamination.

C3.58 Many materials are structurally altered by the radiation process; they may become hardened and embrittled, or discoloured, for example.

C3.59 These radiation induced changes may be beneficial or disadvantageous to the subsequent performance of the packaging or they may simply be aesthetically unacceptable, for example the yellowing which occurs with some PVC materials.

C3.60 Many polymers are now available specifically formulated with stabilisers which make them suitable for use in irradiation processes. The adhesives used to seal packages must also be considered for potentially adverse effects of the radiation.

C3.61 For most hospital users, with only small numbers of items to be irradiated, the advice of the sub-contractor providing the irradiation sterilization service should be sought. Based on their experience of radiation sterilization of similar products they will often be able to suggest appropriate packaging which can be validated by comparison with previously validated products.
Compatibility with the labelling system

C3.62 The importance as labelling as an integral element of the product packaging has been stressed (see paragraphs C1.15 and C2.19 to C2.30).

C3.63 Labelling may take a number of forms, including:
- labelling printed directly on the packaging;
- printed labels attached to the surface of the packaging by adhesive, etc.

C3.64 Whether labels are printed directly on the packaging or onto discrete labels which are subsequently attached to the pack, the labelling system should:

a. not adversely affect the compatibility of the packaging with the sterilization process to be used, for example by excessively restricting the porous area available for gas exchange;

b. not be rendered illegible by the sterilization process to be used;

c. not employ ink of a type which may
   (i) transfer to the pack contents;
   (ii) react with the packaging to impair its utility;
   (iii) change colour and render the label illegible;
   (iv) interfere with the sterilization process by, for example, evolution of volatile components.

C3.65 Labels fixed to the surface of the packaging must be able to withstand exposure to the sterilization process and the defined storage and transport conditions without becoming detached.

C3.66 Given the low cost of computerised label printing systems there can be little justification for using hand-written labels with the inevitable variation in legibility that this causes.

C3.67 Writing on the packaging also presents an unacceptably high risk of causing damage to, for example, paper packaging, which may not be readily visible but is sufficient to breach the microbial barrier properties of the material. Furthermore, some pens, such as ‘felt-tip’ pens and ‘marker’ pens, have inks which may release volatile components in sufficient quantities to interfere with the correct functioning of a steam sterilizer.

Compatibility with requirements for aseptic opening

C3.68 Failure to consider adequately how a pack is to be opened and the contents removed may significantly increase the chance of contamination occurring. With inadequate provision for aseptic opening a $10^{-3}$ probability of contamination is easily possible which compares unfavourably with a $10^{-6}$ probability of sterility required as a minimum standard before labelling a product as sterile (EN 556).

C3.69 The means of sealing or closing the pack should be tamper evident in order that the user may rely upon the integrity of the contents.

C3.70 For sterile products the other major consideration at the point of use must be the ability to remove the product from the packaging without it becoming contaminated with micro-organisms, in other words the aseptic removal of the product.
The provision of aseptic removal may be influenced by a number of elements in the design of the packaged product including:

- the type of product;
- the packaging system chosen;
- the method of closure or sealing;
- the number of layers of packaging material;
- the arrangement of the contents of the pack;
- the use of special equipment to remove the contents.

Sterile medicinal products include both parenteral and topical preparations. The former are predominantly aqueous solutions whereas the latter may be aqueous solutions, oils, emulsions (ointments or creams), or dry powders.

The packaging system employed for sterile medicinal products will normally consist of a closed rigid or flexible container as the primary pack. This may be closed by being hermetically sealed or by being sealed with a penetrable (or removable) elastomeric closure (such as a bung, stopper or disk) held in place with a screwed cap or crimped overseal.

Sterile medicinal products are usually best presented in single-use form. Where a multi-use presentation is employed there will be a requirement for a suitable preservative to be included in the product formulation.

The primary pack may need to be overwrapped if it is necessary to provide for aseptic handling of the primary pack.

Sterile medical devices may be presented as single items such as individual instruments, dressings, etc or, as a single pack containing multiple items; the composition of which is designed so that contents comprise the items required for one (or more) particular procedure(s).

These are commonly described in a variety of terms such as:

- Basic packs (dressing packs which may or may not contain instruments);
- Composite packs (instruments, dressings and other equipment/utensils);
- Supplementary packs (which include instruments, utensils, dressings for use with basic packs and composite packs);
- Procedure packs (which contain all the instruments, drapes, dressings and utensils required for a particular procedure);
- Linen packs packs (which contain all the drapes required for a particular procedure);
- Gown packs, dressing packs, etc.

The packaging system employed for sterile medical devices may consist of flexible or rigid packaging, or the two types used in combination; and may be intended for single use, or be re-usable or a be combination of single use and re-usable.

These may be closed by heat-seal, adhesive, compression gaskets, or tortuous path closures. A common format used in hospital SSDs is a pack formed from a rigid tray wrapped in a flexible packaging material. The tray may be re-usable metal or plastic, such as polypropylene, or single use, such as metal foil, moulded pulp, folded cardboard.
C3.80 For medical devices the arrangement of the pack contents will be of importance. The contents generally are arranged so that when the pack is opened they are available in an order convenient to the user for the intended purpose and suitable for aseptic removal.

C3.81 The method of opening the sealed or closed pack and/or removing the contents affects the aseptic removal capability. The various sealing and closing methods may involve particular risks with regard to transfer of contamination from the outside surface of the pack, or to transfer of fragments of the packaging.

C3.82 Tortuous path seals formed by the folding of flexible packaging material may be constructed so that they may be opened without touching the inner surfaces.

C3.83 Pealable seals are used on heat sealed, and some adhesive-sealed, flexible packs and on many commercially produced packs, for example lidded blister packs. The construction of the seal should allow the opposing surfaces to be grasped easily and the seal on separating should not cause fibre shedding by, say, the splitting or tearing of either surface.

C3.84 Both flexible and rigid packaging systems are used which are intended to be broken, cut or torn open, for example ampoules, paper bags and pouches. It is important that this can be done without introducing contamination into the pack contents either from fragments of the packaging (for example glass particles from an ampoule), or from instruments used in the opening procedure, such as scissors for cutting open paper bags.

C3.85 Rigid re-usable containers for dry goods should have a tamper evident seal which must be broken before the container can be unlatched and the lid opened.

C3.86 Both single-use and re-usable containers for liquids, particularly those intended for topical administration or laboratory use, may have a seal which is formed from a compressible gasket (for example a rubber wad or stopper) held in place by, or as an integral part of, a screw capped lid. Aseptic removal of the contents will depend not only on the ease with which the cap and gasket can be removed but also on the method used subsequently to dispense the contents, for example pipetting, pouring.

C3.87 Both single-use and re-usable containers for liquids, particularly those intended for parenteral administration, may have a seal which must be punctured and penetrated by a suitable device to remove the contents, for example using a hypodermic needle and syringe to remove the contents of a vial.

C3.88 The potential risk of introduction of contamination from surface of seal should be considered. The external surface of the seal may need protection (overseal) which can be removed immediately before use, or the instructions for use may require pre-treatment of the seal surface, for example by swapping with a 70% m/v aqueous solution of spore-free isopropanol.

C3.89 For re-usable systems the ability of the closure to re-seal after each penetration will be an important consideration in the maintenance of sterility.

C3.90 The seal for either single-use or re-usable systems must be of a material which will not be damaged by the penetrating needle to the extent that fragments of the closure will contaminate the contents of the container.
C3.91  Sealed packs should always be carefully inspected for seal integrity, or adventitious contamination, before being opened and this requirement should be drawn to the users’ attention both in the labelling of the pack and on any instructions for use or training programme which may be given.

Compatibility with the contents

Medical devices

C3.92 The suitability of the packaging for use with the particular medical device should be established. This should include limiting values for physical characteristics of both the medical device as well as the stresses which will be imposed during sterilization and subsequent transport and storage.

C3.93 Factors to be considered include, but are not limited to:
- the mass and configuration of the medical device to be packed;
- the presence of sharp edges or protrusions;
- the need for mechanical and other protection;
- interactions with the packaging materials.

C3.94 Consideration of product interaction should also include physical contamination with the packaging material. Small particles introduced into the body during, for example, surgical procedures are widely reported to cause clinical problems including inducing adhesions, granulomata and foreign body reactions in tissues.

Medicinal products

C3.95 Factors to be considered include:
- interactions with the packaging materials, including adsorption, absorption and chemical reactions with components of the packaging materials, for a period not less than the specified storage life under the specified storage conditions;
- adverse effects on the contents due to gas or water vapour permeability, such as permitting loss of water from a formulation, or permitting the ingress of oxygen and subsequent oxidation of one or more components of the formulation.

C3.96 Materials used for packaging should be compatible with the contained product. For example packaging intended for use with parenteral fluids should not shed particulate material to an extent which could compromise the quality of the parenteral being administered.

Laboratory products

C3.97 Factors to be considered include all those noted in the two previous sections for medical devices and medicinal products.
Toxicity

C3.98 Packaging materials and/or systems should not release material known to be toxic in sufficient quantity to cause a health hazard either before, during or after sterilization under the specified conditions of use.

C3.99 Evidence that the packaging material and/or system does not either contain material known to be toxic, or contain material which may react during the sterilization process to form a substance known to be toxic, in sufficient quantity to cause a health hazard is normally sufficient to meet this requirement.

C3.100 Manufacturers of packaging are aware of this requirement and should be able to provide evidence that the formulation of the packaging has been reviewed by a competent toxicologist and found to meet this requirement.

Biocompatibility

C3.101 The biocompatibility of the packaging should be assessed with regard to the intended use of the pack contents. If particular requirements for the product to be sterilized, for example freedom from particulate matter, cannot be established from the material specification for the packaging under consideration expert advice should be sought. In the first instance this advice should come from the manufacturer of the device, who has a legal obligation to specify any particular requirements for the safe sterilization of the product.

C3.102 Test methods for bio-compatibility are described in EN 30933-1; they require the services of a specialist laboratory.

Preservation of sterility

C3.103 The packaging materials and/or systems assembled in the form in which it will be presented to the sterilizers, when assembled, stored, transported and used in accordance with the producer’s instruction, should preserve the sterility of the contents from the time at which they are rendered sterile to the expiry date specified by the manufacturer and/or the point of use.

C3.104 Preservation of sterility is achieved by preventing the ingress of micro-organisms. Many factors affect the probability of such ingress occurring. These include, but are not limited to:

- the concentration of micro-organism in the environment;
- the size of particle on which the micro-organisms occur;
- environmental conditions of temperature, humidity and pressure;
- the rate of change of these environmental conditions;
- flow rates through the layers of packaging material;
- pore size and other filtration parameters of the packaging material.

C3.105 There is no universally applicable, single test method which can be used to establish the microbial barrier properties of a pack.

For particular types or sizes of pack there are tests which may be of value as an overall monitor of microbial barrier properties.
C3.106 For most practical purposes it is necessary to infer satisfactory microbial barrier performance from a combination of tests designed to test attributes of the packaging which are related to microbial barrier properties, for example to test the gas tightness of seals.

C3.107 The time for which any packaging system will maintain the sterility of the pack contents is event related not time related. It is therefore necessary to define, and control, the conditions for both storage and transport, within which the pack will maintain the sterility of the contents.

Storage and transport of sterile packs

C3.108 It is necessary to ensure that the packaging is able to provide the protection necessary to maintain the performance characteristics of:

- the packaging during storage and transport under the specified conditions;
- the contents during storage and transport under the specified conditions.

C3.109 When handled according to instructions, the packaging should protect the product from physical damage and maintain the sterility of the medical device up to the point of use.

Number of layers of packaging material

C3.110 Products may be packaged in a single layer of packaging material, or in multiple layers. Multiple layers of packaging may be used to reduce the likelihood of contamination during storage and when the pack is opened.

C3.111 When two layers of packaging are used to facilitate aseptic removal of the contents:

- the outer wrap is sealed and acts as a barrier to microbial penetration to the product from the environment,
- the inner wrap may, or may not, be sealed and may, or may not, be intended to be a barrier to environmental microbial contamination. It acts as a protective cover during removal of the product.

C3.112 When the inner wrap is a microbial barrier it may serve to provide additional assurance of the maintenance of sterility.

C3.113 This inner wrap, having been maintained in a sterile state by the presence of the outer wrap, may be handled by persons, wearing sterile gloves and about to undertake an aseptic procedure.

C3.114 Moulded plastic shields covering hypodermic needles, plastic end-caps on intravenous administration sets are two examples of inner wraps found on commercially sterilized products. They may also serve additional functions unrelated to the sterile nature of the product, such as mechanical protection, protection of operators from hazards associated with the product etc.

C3.115 Double wrapping is essential for equipment that will be used in an aseptic environment such as an operating room or a protective isolation unit.

C3.116 In particular instances, triple-wrapped product may be necessary to permit the adoption of procedures with a high level of assurance that there will be no contamination, for example transfer of laboratory products into a sterility
test containment facility or transfer of equipment and components into an aseptic manufacturing environment.

C3.117 Single wrapping may be more economical and appropriate when the product, although sterile, will not be used in an aseptic environment and will not be used parenterally or to penetrate tissue, for example Ryles tubes, oesophageal and suction tubes, urine bags, rectal examination sets etc.

C3.118 The various layers of packaging may be used to provide for different functional requirements, for example many surgical instrument and dressings packs are wrapped with an inner layer of paper or cloth which is used to provide a sterile field when opened onto a table, trolley or tray at the point of use.

C3.119 Two or more layers of packaging may be used together to provide a functional requirement which neither alone could meet, for example a single layer of textile may not be an adequate barrier to microbial penetration but two layers in combination may provide satisfactory performance.

Primary and secondary packaging

C3.120 If two layers used together are needed to meet a basic performance requirement then layers both together constitute the primary pack.

Secondary packaging

C3.121 Several individual units, each wrapped in its own primary packaging, may be packed together in a “shelf pack” which may consist of a carton, plastic film wrap, film-wrapped carton or similar.

C3.122 For distribution, multiples of individual units or shelf packs may be packed in transit containers.

C3.123 These may be intended as single-use, for example fibreboard cartons or re-usable, for example plastic or aluminium boxes. Their primary function is to withstand the predictable risks arising during transport and distribution.

C3.124 Some or all of the secondary packaging may be applied before sterilization, especially in commercial sterilization. When this is the case the packaging, in its entirety as presented to the sterilization process, must meet the requirements for sterilization compatibility.

C3.125 When re-usable transport containers are employed, a documented and monitored procedure for maintaining them in a clean, hygienic condition and a good state of repair is necessary.
C4.0 Packaging materials and systems

C4.1 The following section summarises various packaging systems and materials that are available, including methods of effecting suitable seals or closures, their suitability for use with sterilization processes which may be employed by hospital users, and equipment necessary for their effective use.

C4.2 The summary is wide ranging and comprehensive, but not exhaustive. The absence of a particular system or material should not be taken as implying that it is unsatisfactory for use, nor should the inclusion of a particular system or material been seen as an endorsement of its use.

C4.3 The choice of suitable packaging systems and materials will be based on a number of factors. These include, but are not limited to:

- compatibility with available sterilization processes and other factors (see paragraph C3.5);
- particular requirements of the user;
- availability and cost of suitable automatic equipment for filling, sealing, labelling;
- availability and cost of suitable re-processing facilities for re-usable packaging;
- availability and cost of suitable disposal methods for used single-use packaging;
- standardisation of packaging systems within a single production unit.

C4.4 There is no one packaging system that is “correct” for all applications; and for any particular application there may be several systems available none of which is perfect. It may then be necessary to prioritise the requirements to be met by the packaging and select the system which most nearly meets these requirements (Table C2). The two characteristics which are afforded the highest priority most often are compatibility with the sterilization process and maintenance of sterility in storage and distribution.

Sterilization compatibility

Steam sterilization

Wrapped goods and porous loads

C4.5 Goods are normally double wrapped; at least one of the layers will usually be a sheet of paper, paper bag or paper/plastic pouch.

C4.6 The inner lining may be chosen primarily for its absorbency in order to retain condensate in a position from which it will be successfully evaporated during the drying stage of the sterilization cycle.
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<td>Papers Plastic/paper pouches Cellulose/synthetic wraps Spun-bonded polyolefins up to 121°C</td>
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<td>Glass bottles Glass vials/ampoules Plastic bottles Plastic pouches</td>
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</tr>
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* The same packaging materials are also suitable for use with LTS disinfectors

**Fluids in sealed containers**

C4.7 Glass or plastic bottles, vials or ampoules are used for rigid containers and plastic pouches, usually a laminated construction to optimise the performance characteristics, are suitable for flexible containers.

**Dry heat**

C4.8 Aluminium cans or tubes, glass tubes or jars, each of which may be sealed with push on caps, screw caps or crimp-on foil caps, are suitable for dry heat sterilization. Crimp-on foil caps with a pre-printed colour change indicator are also available.

C4.9 Items may be wrapped in heavy or light gauge metal foil or, for items such as laboratory glassware the foil may be used simply to seal the open end of the product.

C4.10 Plastic bags of the sort sold for roasting meat in domestic ovens may also be suitable.
Packaging may consist of paper, used as plain or creped wraps, or in the form of bags or, in combination with plastic film as pouches.

Light cardboard boxes, or corrugated polypropylene boxes, adequately vented and overwrapped with paper or other material as a bacterial barrier are also suitable. When particularly delicate instruments are to be processed the use of an open cell foam for support and protection is acceptable.

The quantity of packaging should be kept to the minimum possible.

Polythene/polyester/nylon or metal foil may be used. The material may be non-porous and gas impermeable which gives good microbial barrier properties. Paper, spun-bonded polymers and non-wovens can also be used but lose the advantage of a process that can deal with impermeable packaging.

For ethylene oxide sterilization a high permeability to air, steam and ethylene oxide is essential.

Paper bags or plastic/paper pouches are usually found to be most convenient for small articles. Wrapping in sheets of plain or crepe paper, or textiles, may be required for large procedure trays containing endoscopes or other thermolabile equipment.

Moulded foam inserts may also be used to provide protection for sensitive equipment such as endoscopes.

Polythene bags with gas exchange ports of Tyvek are also suitable.

The basic requirement is for a material which will not allow the product within the pack to be contaminated by the ingress of microbes in the environment from the time that it is removed from the sterilizer, during transport and storage up to the point of use.

With a non-porous material, where gas flow through the material can only occur through diffusion, the material itself will be an absolute barrier to microbial contamination. The microbial barrier properties of the pack will then depend on the adequacy of the seal or closure. For example, an ampoule, if correctly sealed by fusion, and having no cracks or other flaws, will be an absolute barrier to microbial contamination.

When a porous material is used the barrier to microbial penetration will not be absolute; there will be always a finite possibility of a micro-organism penetrating the barrier and potentially contaminating the pack.
The probability of a micro-organism penetrating the barrier will depend on many factors, including, but not limited to:

- the rate of air flow through the web, which may be influenced by the rate and extent of environmental changes in pressure and temperature;
- the relative humidity, which can affect both the pore size and surface charge of natural fibrous materials (paper, linen etc);
- the type and number of micro-organisms in the environment;
- the form in which they are presented, for example as single organisms or, as they are more usually found, on relatively large particles such as skin squames;
- the nature of the product, which may influence whether contaminating organisms can survive or multiply.

The effect of these various factors is not the same for all materials. For example some porous materials are better at excluding particles of a given size at very low flow rates while other materials perform best at higher flow rates.

It is apparent that the storage conditions will also be a controlling factor in the maintenance of sterility. Dirty, damp conditions can give rise to high microbial counts in the environment; large and rapid changes of temperature, and changes of pressure (including the slamming shut, or violent opening, of doors) will lead to an exchange of air between the contaminated air of the environment and the interior of the pack.

The ability to maintain sterility is primarily “event related” rather than “time related”, although even under controlled conditions there is a greater probability of an adverse event having occurred after prolonged storage.

The most sensitive time for contamination through porous wrapping material is when steam sterilized product has been removed from the sterilizer and is cooling down. During this process air will be taken into the warm and humid environment in the pack.

Materials used in packaging

The materials of which the packaging is made will necessarily limit the sterilization processes with which it is compatible as well as affecting its ability to meet other performance requirements.

Performance requirements for packaging materials include:

- permeability to air, steam and gaseous sterilants, (although this does not apply to materials intended for use with aqueous fluids in sealed containers, dry-heat sterilization by hot air or sterilization by ionising irradiation);
- resistance to penetration by micro-organisms from the surrounding environment;
- resistance to punctures, tears and other mechanical damage which would breach the barrier to microbial penetration;
- freedom from loose fibres and particles;
- freedom from toxic ingredients and non-fast dyes;
• compatibility with the contents under the proposed sterilizing conditions;
• compatibility with the sterilization process to be used, that is, not degraded by it.

Textiles

C4.29 Textile fabrics are used for packaging; traditionally these are woven cotton materials but may also be cotton/polyester blends.

C4.30 Specialist fabrics are also available which may be intended to be water repellent while at the same time being gas permeable. This may be achieved by several means, for example a particularly tight weave of polyester fibres, or a laminated construction with a middle lamella of a suitable polymer film. Care needs to be exercised in using these fabrics that the flow rate of both air and steam through the fabric is adequate for the sterilization process.

C4.31 Textiles are often used as a wrapping material for heavy packs, especially of theatre instruments, which are to be sterilized in a porous-load steam sterilizer.

C4.32 Textiles are stronger than paper, and stronger than many non-wovens, and will resist tearing and rupture.

C4.33 However, textiles are generally a less efficient bacterial barrier than sterilization grade wrapping paper and should always be used in two or more layers. The second layer may be a textile wrap also or a suitable sterilization grade wrapping paper. Alternatively, a sterilization grade paper bag may be used to enclose the textile-wrapped pack.

C4.34 Textile wraps are re-usable.

Papers and non-wovens

C4.35 Both papers, which are made from cellulose fibres, and non-wovens, made from a combination of cellulosic and synthetic fibres, may be used. Both types are suitable for porous-load steam sterilization and most gas processes because they are permeable to air, steam and other gases.

C4.36 The original papers used for steam sterilization wrappers were kraft papers produced for general purposes. Purpose made papers with better controlled porosity and microbial barrier properties, and with enhanced wet strength and water repellency are now used. These are available as plain sheets, creped sheets which give better drape characteristics, as bags and in combination with a plastic film as pouches (or reel material from which pouches can be made).

C4.37 Good drape and handle characteristics are also provided by crepe paper (BS 6254 1989).

C4.38 Plain papers may be used as wraps or preformed into bags or pouches. The bags and pouches may be plain sided or may be gusseted to accommodate bulky items.

C4.39 Wet strength and water repellency are specifically improved over "normal" papers by the impregnation of the paper with high wet-strength resins.
The water content of the paper may be maintained at a relatively high level, thus improving the feel and drape of the paper and minimising superheating due to exothermal rehydration, by the addition of humectants such as sorbitol.

Over many years experience the various forms of paper packaging have been demonstrated to provide an effective microbial barrier.

Non-wovens are generally less effective as a microbial barrier and may need to be used in, or as one of, two layers; they are however generally softer with better handling and drape characteristics.

British Standards exist for all the paper packaging materials and should be used as the basis for purchasing specifications. (These standards will be replaced in due course with European Standards currently in preparation; the draft standards cover the same range of requirements as the existing standards.)

Non-woven materials, made from a combination of natural and synthetic fibres are also widely used. These are often used where otherwise re-usable textiles would be used. They are generally of greater porosity than paper wraps and for this reason may not be as effective as a microbial barrier. They have higher tear and puncture resistance and are softer with better drape qualities. They may also show extremely good water repellency.

**Synthetic materials and laminates**

Polymeric materials, or plastics, may be used in the manufacture of rigid, semi-rigid, or flexible packaging systems.

They may be in the form of sheet or film, which is non-porous, or be produced as a spun-bonded or non-woven sheet which is porous.

Plastic materials are also used in the manufacture of moulded containers, for dry products or for liquids.

Film or sheet material may be an absolute barrier to microbes if it is free from pinholes. Although it may be non-porous that does not necessarily mean that it will be impermeable. Most polymers have some permeability to gas, air, and water vapour. The extent of the permeability varies with temperature, concentration gradient of the diffusing substance etc and although generally low may be important, for example in the long term storage and stability of a pharmaceutical product.

Plastic materials are generally robust and resistant to tearing. The extent to which they show puncture resistance depends much more on the polymer and film thickness used. There have been in the past major problems with thin-film moulded polyethylene commercially produced packs being breached by the sharp edges of the product within.

Plastic materials can usually be heat-sealed to give a high-integrity barrier.

**Polyethylene (polythene)**

Polyethylene is effectively impermeable to air and water and is not suitable therefore for general use in ethylene oxide sterilization processes without special precautions. However very thin films (up to 0.076 mm) thick allow the passage of ethylene oxide (by dissolving in the thin film and then
evaporating from the inner surface). Paper laminated with a thin polythene film may thus be used to provide a heat sealable paper for use in ethylene oxide sterilization.

C4.52 High-density polyethylene is produced as a spun-bonded, non-woven (known commercially as Tyvek) paper-like material. It is very tough, and although it is porous like paper it is water repellent.

C4.53 In commercial use it has been found to provide a satisfactory bacterial barrier. It is frequently used in packs which are to be ethylene oxide sterilized and may be used with a clear film in the form of a pouch, as venting panels in impermeable bags made of, for example polythene, or as a sealing lid on blister packs.

C4.54 It has also been found suitable for use in steam sterilizers operating at sterilization temperatures up to 121°C.

C4.55 It has some disadvantages in that it may attract dust and fibres owing to its electrostatic character, it can be difficult to print on and also it may be difficult to seal, although these latter difficulties largely can be overcome by using non-oil based inks and lacquering with a suitable heat-seal lacquer, respectively. It is also expensive compared with paper.

C4.56 At temperatures above 125°C even high-density polythene has softened too much to be used on its own as an effective packaging material and it is therefore unsuitable for steam sterilization at 126°C or 134°C of for hot-air sterilization.

C4.57 Polythene can be sterilized by ionising radiation.

Polyester

C4.58 Polyester, in the form known as oriented or crystallised polyester, is used as a laminate with polythene in the construction of paper/plastic pouches and reel material.

C4.59 The polythene forms the inner surface which is heat sealed to the paper. The outer layer of the plastic laminate is polyester which gives the required mechanical strength at elevated temperature as well as a good printing surface.

Polyvinyl chloride (PVC)

C4.60 PVC generally has a very low stability to both heat and ionising radiation.

C4.61 PVC will absorb ethylene oxide in large amounts. This is exacerbated by the ethylene oxide combining with the phthalate plasticiser, from which it is aerated only very slowly under ambient conditions.

C4.62 Some grades of PVC are used for the moulded bases of commercially available blister packs.

Polypropylene and polycarbonate

C4.63 Both polypropylene and polycarbonate are relatively heat stable materials.

C4.64 Polypropylene has a very low permeability to air, moisture and ethylene
oxide. It has been used extensively, either separately or in combination with other polymer laminates, as flexible, semi-rigid or rigid containers for heat sterilization of water and aqueous fluids.

C4.65 Polypropylene has been laminated with aluminium foil for use as packaging for wet or oily materials such as skin swabs, alcohol wipes.

C4.66 Polycarbonate has been used extensively for the manufacture of autoclavable laboratory bottles (at 121°C).

C4.67 Certain grades of polypropylene, specifically formulated for the purpose, can be radiation sterilized.

Nylon

C4.68 Nylon is heat stable, and is also steam permeable but it is impermeable to air. Packaging constructed entirely from nylon film is unsuitable for steam sterilization because the air retained in the package may interfere with effective sterilization. It may however be used effectively in combination with a porous material, such as paper, to form a steam-sterilizable pouch.

Glass containers

C4.69 Glass containers, are usually in the form of ampoules, vials, jars or bottles and come in a variety of capacities and shapes, with several different closure systems.

C4.70 Three different grades of glass are available.

a. Soda glass is normally the cheapest (also referred to as Grade I). It is subject to hydrolytic attack particularly when autoclaved containing aqueous solutions. Solutions sterilized in bottles made of soda glass may become contaminated with reactive silicates and show an increased pH. Such bottles are rarely intended for more than a single use.

b. Sulphated soda glass, also referred to as Grade II, is soda glass which is protected against hydrolytic attack by a surface coating of sulphate. The coating is normally applied by sublimation of ammonium sulphate onto the surface of the hot glass concurrently with annealing during the manufacturing process. Bottles made of sulphated soda glass are rarely intended for more than a single use and, if re-used, the sulphate coating is eventually lost and the glass is once again subject to hydrolytic attack.

c. Borosilicate glass, also referred to as Grade III, is much more resistant to hydrolytic attack than Grade I or II glass and is generally the preferred material for containers which are to be used for autoclaving aqueous solutions. Providing there is a suitable cleaning process compatible with the intended end-use, bottles made of borosilicate glass may be re-used a number of times.

C4.71 Borosilicate glass also has better thermal shock resistance characteristics than soda glass when used in a similar container.

C4.72 Glass containers may also be used for dry heat sterilization, and can withstand radiation sterilization. However, irradiation causes a darkening of the glass which may be aesthetically unacceptable.
Metals

C4.73 Metals are used in the fabrication of sterilization containers for use in both steam and hot-air sterilization processes, and to a lesser extent in gas processes such as LTSF or ethylene oxide. Since the material is neither porous nor permeable it must be constructed with a suitable venting system for use in sterilization processes other than dry heat or radiation.

C4.74 The choice of metal should be based on consideration of both its corrosion resistance to the sterilization process, for example in a steam atmosphere, and on its thermal characteristics. The ideal material would have a high thermal conductivity and a low heat capacity and would attain the required temperature quickly, uniformly and without the formation of excessive amounts of condensate.

C4.75 In practice, the choice is usually between aluminium, anodised or otherwise surface treated to give it suitable corrosion resistance, and a suitable grade of stainless steel.

Single-use packaging

C4.76 Both flexible and rigid packaging systems are available which are intended for single use.

C4.77 The recently enacted medical device regulations (see Chapter C2) include a requirement that sterile medical devices be designed, manufactured and packed in a non-reusable pack and/or according to appropriate procedures to ensure that they are sterile when placed on the market. There is thus a clearly stated preference for single-use packaging as the primary packaging for sterile medical devices.

Paper or textile wraps

C4.78 For wrapping materials two different folding methods have been adopted, both of which, when correctly executed, provide a suitable tortuous path to prevent the ingress of contamination.

C4.79 For large packs the parcel fold is the preferred method (see Figure C1).

C4.80 The pack contents are placed on the wrap, approximately in the centre of the wrap. The long edge of the contents should be aligned parallel to the long edge of the wrap.

C4.81 One of the long edges of the wrap is folded over the pack contents to overlap the centre line, and the edge of the wrap is turned back on itself. The fold made by the turning back of the wrap should overlap the centre line of the contents.

C4.82 The opposite side of the wrap is then folded over pack contents to overlap the centre line (and the side already folded over the pack contents), and the edge is turned back on itself.

C4.83 The ends beyond the short side of the contents are then folded to a point and each is then folded over the contents.

C4.84 The same procedure may then be repeated for an outer wrap(s).
Figure C1
Diagrammatic representation of method for closing paper, non-woven or textile wrap using the parcel fold
The wrap is secured in position using pressure-sensitive adhesive tape (high-temperature masking tape or autoclave indicator tape) or by tying with tape or cords.

For smaller packs the envelope fold is preferred (see Figure C2).

In the envelope fold method the contents are placed on the wrap diagonally and slightly off the centre line.

The section of the wrap with the shorter corner-to-pack length is folded over the contents by bringing the corner to the centre.

This is repeated with the corners to the right and left of the first folded corner.

In each case the corner is turned back to provide a flap for opening.

Finally the larger fold is brought over the top and tucked in under the earlier folds with a corner protruding, to facilitate aseptic opening.

The envelope fold if properly executed is quite secure without further attention but if preferred may be secured also with tape or by tying.

**Paper bags, paper/plastic pouches**

**Folding**

Folding is the simplest method to obtain a satisfactory closure for both pouches and bags, although it may not be convenient for high volume production (see Figure C3).

The corners at the open end of the bag or pouch are folded diagonally to give mitred corners.

The top of the bag or pouch is then folded over three times in succession and secured in place with a piece of high-temperature masking tape, or autoclave indicator tape.

The folded top should always be secured with tape; staples should never be used because of the holes that are then made in the package.

The folded top may be opened by cutting through the bag or pouch with a pair of sterile scissors. For non-critical applications it may be torn open; it should not be opened by removing the tape and unfolding the closure.

**Self-seal**

Self-seal bags and pouches are closed by folding as described for plain top bags and pouches, above. However the bag or pouch is manufactured with an impact adhesive coating in a small area of the paper, which is protected before use by a piece of "release paper".

When the bag has been filled the top is folded over as previously described, the release paper is removed and the adhesive patch is pressed onto the surface of the bag to secure the folded top in place.

**Heat seal**

Paper bags and paper/plastic pouches and reel material are available in forms suitable for heat sealing.
Diagrammatic representation of method for closing paper, non-woven or textile wrap using the envelope fold and seal with tape.
**C4.101** The melting point of the heat-seal will effectively limit the maximum temperature at which the pack can be used. Heat-seal packaging should not be used at temperatures above those specified by the packaging manufacturer.

**C4.102** Heat sealing is performed by compressing the opposing sides of packaging, coated on one or both inner surfaces with a lacquer, adhesive or polymer film, between heated plates.

**C4.103** Packaging intended for heat sealing may be film coated, grid lacquered, or have an adhesive band.

**C4.104** Film-coated heat-seal packaging has a thin film of a suitable polymer, such as polythene, laminated to the inner surface. When heated this melts sufficiently to fuse with the opposing surface and form a seal. The heat-seal polymer may be laminated to another plastic or to paper. The polymer film, if applied to the paper element, may limit the porosity of the pack.

**C4.105** Grid-lacquered heat-seal packaging has one side, usually the paper, printed with a heat-seal adhesive in a repeating diamond pattern all over the inner surface. Care needs to be taken that the width of the heat-seal is sufficient to ensure that there is a continuous seal across the width of the packaging.

**C4.106** Adhesive-coated heat-seal packaging has a band of heat-seal adhesive printed on the inner surface of the packaging in the area where the heat-seal is to be made. The adhesive is coloured, usually blue, to aid identification of the heat-seal area.

**C4.107** The seals need to be peelable. They should peel without splitting, tearing or shedding paper fibres since fibres can cause adverse reactions if introduced into open wounds.

**C4.108** Peelability is a compromise between seal strength and the peel characteristics required which can only be achieved by use of the correct heat-sealing conditions.

**C4.109** The heat-seal may be a single line, in which case it should be not less than 5 mm deep and extend across the width of the pack, or a series of lines each about 1 mm wide and 1 mm apart to give a seal width of about 9 mm, with each line extending across the full width of the pack.

**C4.110** The heat-sealing process must be undertaken with care. Creases in the packaging material can result in inadequate or uneven seals.

**C4.111** A weak point in the heat-seal of paper bags may often be found in the corners where the paper is folded back on itself and in gusseted packs where four thicknesses of material become two. This latter problem can be minimised by reverse folding the gusset in the area to be heat sealed, before sealing.

**C4.112** The effect of the sterilization process on heat seals must be considered. The elevated temperatures involved in steam sterilization can weaken the seals. Ethylene oxide gas leaves many seals unaffected but can cause embrittlement of others.

**C4.113** Heat sealing is not only used for flexible packaging. It may be used also on rigid packaging when lids are sealed onto moulded plastic bases. The base tray may be moulded in-line just before filling or may be pre-formed. The
lid may be of paper, Tyvek or other porous material for use in steam or gas sterilization processes or of impermeable film for use with radiation sterilization.

Glass containers

C4.114 Bottles and vials are extensively used for aqueous solutions for use as topical and parenteral medicines, microbiology media, laboratory reagents, in vitro diagnostics, disinfectants, etc which are to be sterilized by moist heat.

C4.115 Glass containers may also be used for hot air sterilization of non-aqueous liquids, such as oils.

C4.116 Containers should never be filled with a volume greater than the manufacturer’s recommended maximum.

Ampoules - fusion seal

C4.117 Two forms of glass ampoule are available; one form intended only for automatic (or semi-automatic) filling and sealing and one which is suitable for manual sealing.

C4.118 Ampoules intended for automatic filling and sealing may be supplied, internally clean, sterile and apyrogenic, with the neck closed by a “bubble” of glass. During the automatic filling process this “bubble” is melted by a flame directed vertically downwards to open the ampoule immediately prior to filling. This normally takes place in an environment controlled to be free from contamination. This type of ampoule is not suitable for manual filling and sealing operations.

C4.119 The relevant DIN standards may be used as suitable specifications.

C4.120 Ampoules are sealed by fusion. After filling, the neck of the ampoule is heated, almost invariably in a gas flame, until the glass softens and the walls of the neck coalesce, surplus unmelted glass in the neck above the point of melting is drawn away and the fused end of the neck is allowed to cool.

C4.121 For any given design of ampoule, the temperature of the flame, the duration of heating and the time and speed at which the surplus neck material is drawn off all affect the quality of the seal. When correctly performed the seal is as strong, or stronger than other parts of the ampoule.

C4.122 Ampoules for use in freeze driers are similarly sealed by fusion.

C4.123 Ampoules are opened by breaking off the neck. This may be facilitated by the inclusion of a deliberate weak point, in the form of a break ring, at the base of the neck during manufacture. Other methods which are available include notching the neck of the ampoule with a glass file, creating a fracture line by the application of a hot wire or rod and several commercially available devices.

C4.124 Whichever method is to be employed, users should be given appropriate instructions and training and should always take precautions to protect their hands from injury due to broken glass.

C4.125 Ampoules are produced to a high level of consistency and faults in sealing are likely to be due to poor setting up or control of the sealing method and rarely, if ever, due to variations in the ampoules.
After the ampoules have cooled, careful visual examination, preferably using a magnifier and a polarised light source, should be used to inspect the seal and any showing cracks, thinning or “blowing” of the seal and sharp protrusions or “tails” of glass, should be rejected.

A vertical drop of 10-15 cm, for example inside a tube of suitable diameter so that the sealed end impacts onto a solid surface, such as a plastic laminate, may also be used to test the ampoule seal. A satisfactory seal will survive, whereas a weak seal will break.

Vials and bottles

As manufactured, glass bottles are generally clean, sterile and apyrogenic. Nevertheless they should be washed before use since they may have become contaminated during packaging and distribution, unless special precautions were taken to avoid this happening.

Screw caps

Screw caps may be made of metal or plastic. They may be used to used to retain in place a separate elastomeric seal, such as a stopper or a wad, or they may incorporate a seal within the cap. In either case the seal is formed by compression of a deformable sealing material between the cap and the glass container. The compressive force applied is a key factor in creating a leak-tight seal.

Metal caps may “back-off” during autoclaving. The differential thermal expansion of the metal of the cap and the glass of the bottle combine to make the cap unscrew slightly during processing. This rarely happens with plastic screwcaps.

The problem can be minimised for metal caps by careful control over the extent to which the cap is tightened before sterilization.

Devices to control the force used to tighten the cap (torque) should be used both to ensure reliable sealing and to minimise the risk of overtightening which can damage the cap or make it difficult to remove

Crimp caps

Crimp caps are metal, or sometimes plastic, capsules used to retain an elastomeric seal, usually in the form of a stopper, in position in the neck of the container.

During the application of the crimp seal, pressure is applied to compress the stopper slightly against the top surface of the neck finish of the bottle. The skirt of the overseal is bent under the base of the retaining rim on the bottle neck by the crimping device. This retains the stopper in place and maintains it under slight compression to provide a good seal.

During steam sterilization of the sealed container the pressure applied by the crimp may be released to some extent by the thermal expansion of the metal capsule. This, and the high internal pressure generated within the container, may cause the seal to leak. It should not be assumed that a seal which is demonstrably leak tight at room temperature will remain so throughout the various stages of steam sterilization.
Re-usable packaging

Textiles

C4.136 Textiles are used in combination with aluminium trays for packs of theatre instruments.

C4.137 The textile wraps should be laundered before each re-use.

C4.138 Control should be exercised over the laundry process to ensure that fabric softeners and fresheners are not used since many of these contain volatile components which will evolve gas during steam sterilization and compromise the efficacy of the sterilization process.

C4.139 The importance of thorough inspection before re-use cannot be over-emphasised. A light table should be used, and wraps with pinholes, clearly visible as points of light, should not be used.

C4.140 The location of the defect should be clearly marked and the item sent for repair by means of a heat-seal patch. Sewn patches are not acceptable because of the needle holes created around the patch.

C4.141 Worn textile wraps are readily discernible since the light will shine through the more open weave that occurs as the fabric wears. These should no longer be used as a sterile packaging wrap.

Containers for solid goods

Impermeable or unvented containers

C4.142 Aluminium tubes with crimped foil caps and larger canisters (made from aluminium, copper or stainless steel) with slide or screw-fit caps may be used satisfactorily for hot-air sterilization. Containers of this sort are used frequently for pipettes or glassware in the laboratory.

Open-topped trays and perforated containers

C4.143 Trays for containing sets of theatre instruments, or similar, are often constructed in aluminium. Plastics such as polypropylene may also be used. The trays may have solid bases and sides or be equipped with drainage ports to allow condensate formed during steam sterilization to run off.

C4.144 When condensate drainage is provided it is necessary to ensure that the condensate is not discharged onto other parts of the sterilizer load, which will then emerge form the sterilizer wet.

C4.145 Trays may be overwrapped in textiles, single-use wraps or bags, or a combination of these materials to achieve the required protection, absorbency and microbial barrier properties.

Instrument orientation trays

C4.146 These trays, usually constructed in metal, are fitted with retaining clips designed to hold a particular set of instruments in position. They are often found in dental practice and also for use with sets of orthopaedic instruments and rigid endoscopic instruments.

C4.147 They are almost invariably fully vented, or unlidded, and in this condition may be suitable for use in a steam sterilizer intended for unwrapped instruments and utensils (see paragraph 3.23).
Dressings drums

C4.148 Perforated metal containers, fitted with a filter material and closable louvres were specified in BS 3281, 1960, for use as “dressings drums”. These were intended to contain dressings and porous goods sufficient for a number of clinical procedures. The product has been regarded as obsolete except for its use, until recently, as a convenient container for towels for the Bowie and Dick test. Even this use has now been discontinued.

C4.149 There is, however, a new generation of re-usable rigid containers intended for use as a packaging system in steam (and in some cases, gas) sterilization processes. These are intended to contain instruments and/or porous goods which will be used in a single clinical procedure. They are thus more akin to the trays described in paragraphs C4.143 to C4.145 than to the obsolete dressings drums.

Re-usable rigid containers

C4.150 A European standard specifying performance requirements for rigid re-usable containers is in preparation. When adopted it will be published as BS EN 868 – 8.

C4.151 Container systems are constructed in a variety of materials and those from various manufacturers differ greatly in design, construction and mode of operation.

C4.152 The containers are constructed from impermeable materials. The joint between the lid and the base is sealed by means of a suitable gasket, which should be accessible for inspection and cleaning between uses.

C4.153 In order to permit the flow of gases (air and steam and, where applicable, sterilant gas) in and out of the container that is required by the sterilization process the containers are fitted with one or more sterilant ports.

C4.154 Two different operating principles are used for the sterilant ports, although both may be used in combination. The exchange of gases may be through a porous filter material or through a valve system.

C4.155 The filter system is little different in principle from the porous packaging systems considered previously. Its compatibility with the sterilization process depends on its porosity and on being able to provide the necessary flow rate through the filter to permit attainment of the sterilizing conditions within the container.

C4.156 The ability to maintain sterility depends on the filter efficacy and whether it is able to exclude particles of a size which may contain viable organisms. The small area of surface available compared with the volume of the pack produces relatively high flow rates across the filter material and this influences the materials which can be used effectively.

C4.157 If a re-usable filter is used then great care is needed to ensure that:

• it has not become partially blocked, thus impairing the flow of gases and compromising the sterilization process;

• it has not been damaged, thus allowing the passage of unfiltered gases which would compromise the maintenance of sterility.
Both re-usable and single-use filters need to be installed correctly so that the filter is effectively sealed in the holder and there is no passage of unfiltered gases around the filter.

The alternative system for sterilant ports is the valve system.

Outside the sterilizer the valve is normally closed and, if the seals on the valves are effective, presents an impermeable barrier to external contamination.

The valve system has to be arranged to open automatically in the sterilizer to permit the exchange of gases between the container and the environment.

A number of systems are used by the various manufacturers but most depend on valves which open in response to a pressure difference between the container and its surroundings. A diagram of the operation of such a system is shown in Figure C4.

It is apparent that a finite pressure difference must exist across the valve before it will open. The magnitude of the pressure difference will depend on the force exerted by the springs keeping the valve closed.

If the pressure difference required to open the valve is too great, the contents of the container will not be exposed to the sterilizing conditions in the sterilizer chamber. The correct functioning of the container is closely related to the pressure change characteristics of the sterilization cycle.

If the required pressure difference is too small the valve will open outside the sterilizer due to changes in ambient pressure and temperature, thus allowing the inflow of unfiltered air from the environment.

Some container systems are also fitted with a valve in the base of the container which is used to allow condensate to drain away, to assist in drying the contents of the container.

The condensate drain valve may be fitted with a thermostatic device to open the valve when it is above a specified temperature, say 80°C, or it may operate on pressure differential as previously described for valved sterilant ports.

After repeated use, the springs controlling a valved system will age and the force exerted by them will change. It is essential that the manufacturer’s instructions for maintenance, testing and replacement of key components such as seals, sterilant ports and drainage valves are followed rigorously.

The performance of either type of container may be seriously affected both by the nature of the sterilization cycle (particularly the characteristics of the air removal phase and the drying stage) and by variations in the quality of services supplied to the sterilizer (for example the dryness fraction of the steam). These variables are sterilizer and site specific respectively.

It is necessary, therefore, to establish, by appropriate on-site testing, that any particular design which it is intended to use functions correctly in the specific sterilization cycle with which it is to be processed, in the sterilizers which will be used in practice.
Figure C4

Diagram to show the principle of operation of valve-type re-usable container systems

Lid

$P_1$  
$P_2$

$P_1 = P_2$
Valve remains closed

Lid

$P_1$  
$P_2$

$P_1 < P_2$
Valve opens to vent the container

Lid

$P_1$  
$P_2$

$P_1 > P_2$
Valve opens to allow air or steam into the container

Note: The above diagrams are intended to be an idealised example of the operation of a valved system. They do not represent any commercially available system.
C4.171 Re-usable containers have a number of apparent advantages. They offer excellent mechanical protection to the contents and a convenient, modular system for storage and distribution.

C4.172 The use of a solid-walled container gives the impression of providing good protection against microbial and other environmental contamination. In practice the barrier properties are dependent on the adequacy of gaskets and seals and the sterilant ports described above.

C4.173 The condition and function of filters, valves, sealing gaskets and locking systems needs to be verified on each container before each use.

C4.174 Between uses containers should be disassembled and cleaned following the manufacturer’s recommendations. These usually suggest cleaning by washing with a mild detergent, either manually or in a washer/disinfector.

C4.175 The choice of detergent should accord strictly with the manufacturers recommendations since a number of cleaning agents in common use can cause corrosion or surface cracking on the metal or plastic surface of containers.

C4.176 These containers are often used to return used and soiled instruments, which are potentially contaminated. Whenever practicable they should be decontaminated and cleaned in a washer/disinfector.

C4.177 Most containers are fitted with interior baskets or mesh trays used to hold the instruments. These may be suitable to contain returned instruments as they are processed through a washer disinfector.

C4.178 In use the containers need to be properly loaded if they are to be used successfully. The manufacturers recommendations concerning the maximum weight, the proportion or density of metal ware or rubber goods and the presence and location of absorptive materials in the load should be followed.

C4.179 Some containers are intended to be used in conjunction with porous packaging materials, either as an inner or outer layer of packaging, whereas others are intended to be used, and will only function correctly, without any other packaging being present during sterilization. It is important that the manufacturer’s instructions are followed.

C4.180 Containers which are not intended for use with a second layer of packaging, that is those which can only function as a single packaging layer, are not suitable for use in an aseptic environment (see paragraphs C3.109ff).

C4.181 Containers manufactured to the proposed European Standard will be sized in relation to the standard loading module for large steam sterilizers (see EN 285). High packing densities within the sterilizer chamber can be achieved and it is important to ensure that the maximum permitted load for the sterilizer is not exceeded.

C4.182 To avoid problems with moisture retention within the container it may be necessary to increase the time allowed for the drying stage of the sterilization cycle.

C4.183 Each container should be fitted with a tamper evident closure system which should provide a clear indication when the integrity of the closure has been compromised.
C4.184 The containers are designed to stack for storage purposes. Containers from any one manufacturer should stack securely but containers of different provenance may not.

C4.185 When purchasing this type of packaging system all the containers should be from the same manufacturer to ensure compatibility.

C4.186 Re-usable containers are often promoted on the basis that they are more cost effective than single-use packaging. A decision based on cost grounds requires careful evaluation of the initial capital cost, cleaning and maintenance costs (including all equipment, components, consumables and labour required), the working life (the number of re-uses) which the manufacturer is prepared to guarantee, the likelihood of damage or loss and the cost of eventual disposal.

Glass containers

C4.187 Bottles intended for single use should not be re-used. Bottles intended for multiple use are available for most applications.

C4.188 Re-usable containers should not be used for solutions intended for parenteral administration.

C4.189 The information given for single-use screw cap and crimp-on closures is equally applicable to re-usable containers, with the following additional requirements.

Vials and bottles

Cleaning

C4.190 Before bottles can be satisfactorily re-used a cleaning procedure is required which has a demonstrated capability to remove any dirt or contamination, as well as any residues from the previous use. It is also important that the cleaning process is well controlled and ensures that there are no residues of cleaning agents.

C4.191 Cross-contamination can be most easily controlled by ensuring that whenever possible re-usable containers are only refilled with the same product, for example by reserving a set of bottles only for sterile water and another set only for sterile isotonic saline and so on.

Inspection

C4.192 Inspection of the bottles after cleaning and prior to re-use should include a careful visual examination of the neck finish. A chipped or cracked neck finish could prevent an adequate seal or lead to the failure of the seal during transport or storage. Bottles that have been damaged in this way should be scrapped.

C4.193 Inspection of the outer surface of the bottle should also be made. Bottles being sterilized are subjected to considerable stress both from the high internal pressures generated and from thermal shock. Scratches or other mechanical damage on the outer surface of the bottle weaken it and significantly reduce the pressure and the thermal shock which can be tolerated without breakage.
One bottle breaking in a sterilizer load may provide sufficient force to cause others to break also. Re-usable bottles with surface damage should be rejected and either used for applications which do not require steam sterilization or be scrapped.

The inspection of the neck finish should also consider any damage to the screw threads or the retaining shoulder on the outside of the neck of bottles which are closed with screw caps or crimped seals respectively.

**Screw caps**

Screw caps, and the elastomer wads, stoppers or bungs used in conjunction with them, are often regarded as re-usable, and many of them may be satisfactorily re-used a number of times.

The screw cap should be separated from any sealing wad and both should be thoroughly cleaned and inspected for damage before re-use.

Metal caps that have been dented, or are showing visible signs of wear on the threads, should be scrapped.

Rubber wads and rubber stoppers should also be carefully inspected for surface damage and any showing cuts, abrasions, staining or permanent deformation should be scrapped.

Plastic screw caps with a built-in seal are also commonly used. These should be inspected very carefully for damage to the thin sealing gasket which is moulded into the inner surface of the cap. Any damage to this area will almost certainly cause the cap to leak.

**Crimp caps**

Crimp caps are not themselves re-usable but the bottles on which they may be used can be. A special tool and some care is needed to remove crimped seals without risk of injury.

The old seal should be discarded. The seals are usually fabricated from aluminium and the metal can therefore be reclaimed.

The elastomer seal should also be scrapped.
C5.0 Purchase, quality control and storage

C5.1 The purchase, handling and control of packaging materials should be given similar attention to that given to components and other materials incorporated directly into the product.

Purchase

C5.2 All packaging materials should be purchased, whenever possible, to a British Standard or other suitable specification from approved suppliers.

C5.3 Packaging material should be purchased only to an agreed, written specification. When it is intended to purchase a catalogue item, the specification for that item should be obtained from the supplier and used as the basis of that purchase, and all subsequent purchases of the material. This should ensure that the user is informed of any changes in specification subsequently made by the supplier.

C5.4 The purchase order should be based on not more than the quantity which can reasonably be expected to be used within the manufacturer’s stated shelf life for the product.

C5.5 Although paper products, and other packaging materials, have a prolonged shelf life the manufacturer’s expiry date may relate to other properties of the product such as a process indicator or an heat-seal adhesive whose performance may deteriorate on storage.

C5.6 The specification and purchase order should require that the material be delivered in unopened containers, using covered vehicles, suitably protected from water damage or soiling and that it is handled with care to prevent mechanical damage.

C5.7 The packaging materials should be supplied suitably wrapped to provide the required protection when it is stored under the specified conditions.

Specification

C5.8 For medical devices and medicinal products, and generally for laboratory products also, the specification should include:

- a description of the materials including:
  - the designated name and any code or reference;
  - the size;
  - the quantity in each unit pack delivered;
  - the reference, if any, to a pharmacopoeia’s monograph, British Standard or other published specification;
  - the approved suppliers, and if possible, the original producer of the material;
  - a specimen of printed materials;
• directions for sampling and testing, or reference to written procedures;
• qualitative and quantitative requirements with acceptance limits;
• storage conditions and precautions including the maximum period of storage.

Quality control

C5.9 In many cases users of packaging materials will lack the facilities necessary to carry out a comprehensive independent assessment of delivered materials for conformity to their purchase specification.

C5.10 Nevertheless every reasonable step should be taken to establish conformity. This requires that each delivery should be examined to ensure that:

• there is no visible damage to the shipment;
• the delivery note, the label description and the purchase order are in agreement concerning the quality, size and number of the material;
• that each consignment has clearly identifiable lot numbers;
• that each lot delivered is accompanied by a Certificate of Analysis or Certificate of Conformity, or if the delivery is a further supply from a lot previously received that the appropriate certificate is on record.

C5.11 When, due to the nature of the packaging or the product, it is necessary to carry out tests, other than a careful visual appraisal, on incoming packaging materials a random sample should be taken and submitted for analysis.

C5.12 There should be a formal sampling plan which should take account of:

• the quantity received;
• the quality required;
• the nature of the material, and the risk involved if the material is not to specification, for example if the product makes contact with the packaging material;
• the established reliability of the packaging manufacturer.

C5.13 The number of samples taken should be specified statistically, in accordance with a recognised standard, such as BS 6000 or BS 6001.

C5.14 In confirming that the material supplied is identical in every respect with the material ordered particular attention should be paid to printed labels and packaging materials.

C5.15 A system for segregating delivery of packaging materials which have not been examined from those which have been found suitable for use should be implemented.

C5.16 Provision should be made for the temporary secure storage, prior to disposal or return to the supplier, of material which was delivered but, on examination was found not to conform to the specified requirements.
Storage

C5.17  Packaging materials should be stored under conditions which are maintained within those specified by the manufacturer of the packaging. This is best achieved by environmental control of the storage area.

C5.18  The temperature, and where necessary the humidity, of the storage environment should be monitored with a maximum-minimum thermometer and hygrometer, even if the store is not environmentally controlled.

C5.19  Paper and other moisture sensitive packaging materials should not be stored adjacent to:

• external walls or other surfaces which may be at a lower temperature than the ambient temperature of the store;
• sources of heat which could cause dehydration of the packaging material.

C5.20  Sheet materials should be stored flat, not on edge.

C5.21  Packaging materials should be stored on shelves, clear of the floor.

C5.22  Pre-printed labels and other printed packaging materials should be stored in secure conditions which exclude unauthorised access and should be transported in separate containers in order to avoid mix-ups.

C5.23  Packaging materials should be issued for use only by authorised personnel following an approved and documented procedure.

C5.24  Outdated or obsolete packaging material, especially printed material, should be destroyed and this disposal recorded.
C6.0 Validation of packaging systems

C6.1 All materials and procedures for packaging should be specified in documented form.

C6.2 Before a particular packaging system is adopted for a product, or group of similar products, it should be evaluated to establish its suitability.

C6.3 This evaluation should be documented.

C6.4 Specific testing may not be necessary when appropriate data are available, historically from similar use (whether by the same or different sterile product manufacturers), from the manufacturers of the packaging system or from an independent third party.

C6.5 The factors that need to be considered for evaluation include, as a minimum, those listed in paragraph C3.5.

C6.6 The compatibility of the packaging with the sterilization process can be established for many packaging systems by demonstrating conformity of the packaging and the sterilization process with published standards, for example sterilization-grade paper bags manufactured in conformity to BS 6257 for use in a sterilizer conforming to BS 3970 Part 3 and operated in accordance with the guidance given in this HTM may be presumed to be compatible.

C6.7 Re-usable containers should be subjected to thermometric performance tests before they are adopted as a packaging system. This may be accomplished using a container modified to provide a gas-tight thermocouple entry port and carrying out tests essentially similar to the small load and full load tests described in HTM 2010 Part 3 paragraphs 13.7 to 13.14 and 13.15 to 13.24 respectively.

C6.8 The tests should be carried out with a container fully loaded with items of the type which it is intended to process. If both instruments and textiles are to be processed the container should be tested under both fully loaded conditions. The full load test should be carried out with the sterilizer fully loaded with fully loaded containers.

C6.9 The temperature profile obtained should not show any delay in the contents of the container equilibrating with the sterilization temperature in the chamber, when compared to the results obtained using a small-load test pack.

C6.10 Load dryness should be verified using either the hospital load test described in HTM 2010 Part 3 paragraph 13.37 or, when quantitative results are necessary, by a modification of the method described in HTM 2010 Part 3 paragraphs 13.25 to 13.36.

C6.11 The compatibility of the packaging with the labelling system will usually be established by using the labelled pack for such tests as may be necessary.
C6.12 The compatibility of the packaging with the user’s requirements at the point of use, for example aseptic opening, should be verified by consultation with the user. Testing is rarely required.

C6.13 The sensitivity of the pack contents to particular risks, such as irradiation, moisture, mechanical shock, static discharge and the compatibility of the packaging with the contents, for example the medical device or medicinal substance, in other words, that the packaging has no adverse effect on the medical device or vice versa, will usually be apparent from historical data. When new products are to be packaged and sterilized, the instructions which the device manufacturer is required to provide should be followed.

C6.14 The protection provided by the packaging against adverse environmental influences which may reasonably be anticipated, such as mechanical shock, vibration, chemical or microbial contamination, may be considered in two stages:

a. First, the extent to which the environment to be encountered during transport and storage may be controlled. Secondly, the protection provided by the packaging.

b. Adequate performance of the packaging should be demonstrated under the anticipated conditions of use by simulating the abuses a pack may encounter during routine methods of transit and storage.


C6.16 The protection provided by the packaging against microbial contamination should also be evaluated.

C6.17 Tests for bacterial penetration of packaging are beyond the experience and competence of most hospital users and could only be carried out by specialist subcontractors. There is no agreement on suitable test methods, or performance standards, for the microbial barrier properties of sterile packs.

C6.18 The microbial barrier properties of a sterile pack are dependent on both the materials of which the packaging is made and the construction of the package.

C6.19 Materials that are impermeable to gases may reasonably be assumed to present an absolute barrier to microbial contamination. When such materials are used in the construction of a pack which is hermetically sealed (for example glass ampoules) the barrier may also be assumed to be absolute.

C6.20 Package testing may be avoided by the compilation of evidence that the materials of construction are themselves an adequate barrier together with evidence that all seals and closures are adequate barriers.

C6.21 Two different approaches have been adopted to testing porous materials for their ability to exclude microbial contamination; tests based on physical particulate retention (for example the methylene blue test specified in British Standards for sterilization packaging) and tests based on the use of micro-organisms (for example the tests specified in German standards for sterilization packaging).

C6.22 For many materials a standard specification has been adopted which specifies the physical and/or chemical characteristics of the material which have
been shown to provide satisfactory performance against a standard penetration test. Whenever possible materials in compliance with one of these standards should be adopted so that purchases are to an agreed specification which will give the required level of assurance.

C6.23 The methods available for verification of the adequacy of the seal or closure depend on the method chosen. Seals formed in impermeable packaging materials can be tested by one of several leak test methods but these are not generally applicable to seals formed in porous materials, nor to closures which rely upon a tortuous path to exclude microbial contamination.

C6.24 Heat seals are also dependent for their success on the performance of the heat sealer used. Several methods for testing heat seals are available but visual examination of the quality and uniformity of the seal from samples of packaging taken before and after sterilization and before and after storage and Journey trials may be sufficient.

C6.25 Closures which rely on a tortuous path formed by folding are very dependent for their success on the skill of the operator forming the closure. There is good published evidence, from a number of studies carried out over many years, that the closures described in paragraphs C4.78 to C4.97 are satisfactory.

C6.26 For packaging materials to be used in gas or irradiation sterilization processes it may be necessary to determine the extent and nature of microbial contamination on the packaging before sterilization. This should not be necessary for steam sterilization processes operating at 134°C for not less than three minutes.

C6.27 When knowledge of the packaging bioburden is required this information should be sought from the packaging manufacturer or it should be determined in accordance with EN 11174 by an appropriately experienced laboratory.

C6.28 When re-usable packaging systems are being evaluated it is important that the cleaning, inspection and maintenance procedures and methods are also evaluated for their ability to consistently restore the packaging system to the required condition for re-use.

C6.29 Before any performance testing is undertaken a test protocol should be prepared. This should document:

- the tests to be performed, including full details of the equipment and methods to be used, personnel etc.;
- the purpose of the tests;
- the sequence in which the tests are to be carried out;
- the format in which the results are to be documented;
- the pass fail criteria for each attribute being evaluated.

C6.30 The test protocol and the written report of the results should form part of the validation documentation.
C7.0 Facilities and environmental control for packaging operations

Packaging operations

C7.1 In SSDs the assembly of components, placing them in primary packaging and sealing or closing the packaging usually is referred to as a “packaging operation”. Thus is in contrast to pharmaceutical and laboratory practice where the same operation is described usually as a “filling operation” and the term “packaging operation” is reserved for the subsequent, often post-sterilization, application of secondary packaging. In the following section “packaging operation” refers to the application of primary packaging and any secondary packaging which is included in the sterilization process.

C7.2 Detailed guidance on suitable facilities is given in Health Building Note 13 - ‘Sterile services department’ HMSO 1992 and Health Building Note 29 - ‘Accommodation for pharmaceutical services’ HMSO 1988.

General requirements

C7.3 All areas used for the reception, inspection, storage, filling, and sealing of packaging require a high standard of finish and cleanliness.

C7.4 Areas where clean, unpacked product is to be handled for, say, assembly and packaging, need a controlled environment to minimise the potential for recontamination of product by, for example mechanical ventilation or gowning procedures.

C7.5 All exposed surfaces should be smooth, water resistant and sufficiently durable to withstand frequent cleaning. The construction and any fitments should be designed to be free from crevices and sharp internal corners, which can trap dirt.

C7.6 Areas where product, ready for incorporation into primary packaging, and primary packaging materials are exposed to the environment for significant periods should be controlled to defined standards of environmental cleanliness.

C7.7 For SSDs there should be a dedicated room where the production of packs, trays etc takes place. This should be a controlled environment. HBN 13 recommends that packaging facilities for SSDs should be controlled to BS 5295 Class L and a detailed summary of the environmental needs of the various areas is provided in HBN 13, Appendix 5.

C7.8 The GMP Guide for Pharmaceuticals recommends that parenteral solutions should be filled under a laminar flow work station (Grade A) within a cleanroom controlled to Grade C.

C7.9 The provision of controlled, clean environments has additional implications for staff hygiene, gowning and entry procedures and the behaviour of personnel within the facility. These requirements are fully described in the relevant GMP guides.

C7.10 Doorways throughout the facility should be wide enough, and free from damaged or rough edges, to eliminate the danger of packs of product on trolleys being damaged as they are wheeled through.
Facilities for packaging operations

Cleaning

C7.11 All operational areas of a sterile-product manufacturing facility need to be maintained to a high standard of cleanliness.

C7.12 Detailed cleaning procedures and schedules should be documented and their implementation monitored.

C7.13 For guidance on suitable procedures and schedules see ISSM Guide to Good Manufacturing Practice for NHS Sterile Services Departments and The DoH MRS Guide to Water and Environmental Cleaning.

C7.14 Surface finishes and cleaning methods must be compatible. Appendix 6 of HBN 13 suggests appropriate finishes.

C7.15 Cleaning equipment and facilities for the storage and preparation of cleaning materials and equipment should be provided separately for areas between which cross-contamination could be problematic.

Cleaners’ room

C7.16 HBN 13 recommends the provision of a dedicated cleaning facility for the packing room, and a separate, dedicated, cleaning facility for the linen preparation area (if one is used).

C7.17 The cleaning facility provides storage for cleaning equipment and materials, a sink or sluice with hot and cold water of the appropriate quality and other facilities needed for the cleaning and preparation of the cleaning equipment. In addition, it usually accommodates consumable items for operational areas which are normally replaced by the cleaner. This would include plastic waste bags, liquid or leaf soap refills for dispensers in changing rooms etc.

C7.18 Hand washing and drying facilities should also be available in the cleaning facility.

C7.19 Whether or not separate facilities are provided, it is necessary to ensure that separate cleaning equipment is used for the assembly/packing area and other areas within the unit.

Sterile services departments - SSD

C7.20 The packing room receives single-use materials from materials’store and reusable goods after the completion of appropriate decontamination procedures.

C7.21 The decontaminated re-usable goods will include components to be incorporated into packs and may include re-usable packaging, such as textiles, instrument trays, re-usable containers.

C7.22 Within each of the areas supplying the packing room, or at the interface between these areas and the packing room there is usually provision of inspection/verification facilities to ensure that all product transferred into the packing room is the correct item and in a suitable condition for use.

C7.23 In the packing room these goods are then assembled into the combinations specified to form the pre-set trays and procedure packs which are required. These are then packed in preparation for sterilization (see HBN 13 paragraph 2.44).
Linen room

C7.24 Cleaning facility - dedicated required same as packing room. Textiles for incorporation into packs may be product items, such as surgical drapes, towels or gowns, or they may be wrapping materials.

C7.25 Textiles for wrapping purposes may be received in the SSD as laundered linen which has already been checked and folded to an agreed pattern or in bulk form, unchecked and unfolded.

C7.26 The SSD has an obligation to ensure that the laundry process is defined and controlled and the quality checks on the textiles to be used are rigorously applied to ensure that the pre-determined standard is maintained, even if the laundry has the devolved responsibility for inspecting the packaging textiles (see paragraphs C4.136 to C4.141).

C7.27 When unchecked linen is provided from the laundry, the SSD will require suitable inspection facilities within a linen preparation room.

C7.28 When textiles are to be used as the primary wrap for sterile packs they have to be inspected to a defined standard, which should include freedom from all tears, cuts and visible holes. A light table is essential for inspection to this standard.

C7.29 When the textiles are used only as an inner wrap and it is intended that the necessary bacterial barrier properties will be provided by an outer wrap of another material, such as a sterilization grade paper wrap or bag, a less rigorous inspection standard may be accepted for the textiles. A large flat surface where the wrap can be fully unfolded and a good standard of ambient lighting are still necessary.

C7.30 The linting of fabrics can be a major problem. Lint is a respiratory hazard and a fire or explosion hazard and together with other dust may contribute to an insanitary environment by providing a vehicle for the transfer of micro-organisms.

Packing room

C7.31 The activities undertaken in the packing area may be summarised as to:

- receive QC released single use, re-usable and consumable items. Note that in some units the QC Inspection on cleaned and decontaminated items is carried out within the packing area. When this system is used, and particularly when inspection is done at the same time as assembly, great care is needed to ensure proper segregation of rejected items;
- assemble items into pre-set trays and procedure packs;
- verify that the contents match the specification;
- pack;
- close and/or seal the packaging system;
- label;
- verify the accuracy of the label;
- transfer to sterilizer.

C7.32 The packing room should be mechanically ventilated to ensure that the particulate count and pressure differentials meet the requirements of BS 5295 Class L in the “unmanned condition”. 
C7.33 Although it may be possible to demonstrate that areas lacking mechanical ventilation can meet the required particulate standard when tested, this is not a satisfactory substitute. Mechanical ventilation is required to ensure that the particulate standard can be met consistently and also to ensure that there is a positive pressure relative to surrounding areas to minimise the ingress of contamination.

C7.34 HBN 13 recommends that the air supply filters should have a minimum resistance of 85% when tested in accordance with BS 6540 Part 1 (EU6).

C7.35 Humidification may also be required to avoid dehydration and subsequent problems.

C7.36 When plastic materials are being used for packaging excessively dry atmospheres can promote a build up of static electricity which causes problems, such as attraction of particulate material.

C7.37 Dry atmospheres may lead also to excessively dry absorbent materials, such as paper or cotton textiles. When steam sterilized the exothermal rehydration of these materials can lead to local superheating and impairment of the sterilization process.

C7.38 Ethylene oxide sterilization requires goods to be sterilized which have been humidified to provide an optimum moisture content. This can be greatly facilitated by the maintenance of appropriate ambient humidity during assembly and packaging.

C7.39 The layout of the packing room should allow an orderly flow of work and should provide sufficient separation between activities to preclude the possibility of mix-ups, mis-labelling etc.

C7.40 Work surfaces should be of sufficient size to allow the largest wrapping materials which will be used to be fully opened without draping over the edges of the work surface.

C7.41 In-line labelling and label printing may be used to advantage, but printers are often noisy. Their location should be considered carefully to minimise the adverse effect of this noise. In addition, when it is necessary for staff to read information displayed on VDU screens it is essential that the ambient lighting is suitable.

Sterilizer loading area

C7.42 When single-ended sterilizers are used it is important to ensure adequate segregation of unprocessed goods from processed goods. Chemical process indicators in conformity to EN 867-2 may be of value.

C7.43 Adequate space must be available for the number and type of trolleys to be used.

Post-sterilization area

C7.44 This area provides the interface between the sterilizers and the processed goods store and should provide adequate space and facilities to allow product removed from the sterilizer to be inspected and to be quarantined until verification that the cycle was satisfactory.

C7.45 The area should provide space where packs may be allowed to cool to room temperature before they are handled.
C7.46 Each pack should then be inspected to verify that the packaging is not wet or damaged and that the seal or closure is intact.

C7.47 For gas sterilization processes an additional facility to provide the controlled removal of residual sterilant gas may be required. After verification that the sterilization cycle was satisfactory and inspection of the sterilized packs they may be transferred to the processed goods store or sent directly to despatch for immediate distribution.

**Processed goods store**

C7.48 The area should provide facilities where sterile packs may be stored away from excessively humid, hot or cold locations, strong light sources and electrical power supplies. Adverse conditions can cause deterioration of plastics, rubber and cellulosic materials found in the packaging or the contents, giving rise to embrittlement, loss of tensile strength, and so on (see SIB(7)3 ‘Storage of sterile medical devices and surgical products’, DHSS 1982).

C7.49 The storage area needs to be clean, dry and well ventilated but free from draughts. Ideally the environment in the store should be maintained at 18-22°C with RH 35-75%.

C7.50 Storage may be on open shelves or in closed cupboards. When shelves are used they may be solid or of wire mesh construction. The lowest shelf should be solid and should be 25-30 cm above floor level. The top of shelving stack should be a solid shelf 25-30 cm below ceiling level to allow room for cleaning, but should not be used for storage.

C7.51 Shelves should be located away from outside walls which can suffer from condensation problems, and from other sources of water such as sinks, and sprinklers.

C7.52 There should be no unlagged cold water pipes or other similar services which may cause condensation to form and drip onto packs.

C7.53 A high standard of cleanliness is required in this area. When facilities are less than ideal the inadequate conditions may be ameliorated by wrapping the sterile packs in a protective dust cover such as a polythene bag during storage. This may then be removed immediately prior to despatch. Note that, if packs are to be wrapped in dust covers, they must be allowed to cool to room temperature first.

**Materials storage**

C7.54 HBN 13 Appendix 4 provides guidance on determining the space required.

C7.55 A materials store is required for the storage of incoming supplies, including single use items, consumables, and new re-usable items as well as packaging materials.

C7.56 The same store may also be used for incoming supplies of commercially produced supplies items (for example commercially produced sterile packs).

C7.57 The passageway between shelves or racking should be wide enough to permit proper use of handling equipment without causing damage to stored materials.
C7.58 Secure separate storage needs to be provided for the segregation of defective or non-conforming materials products.

C7.59 Facilities are required for the reception of purchased goods and subsequent inspection and confirmation that they are supplied in accordance with the purchase specification.

Packaging equipment

Heat sealers

C7.60 Several patterns of heat sealer are in common use:

a. Hand-operated heat sealers with scissor action jaws; many of these were designed for sealing light gauge polythene bags for food use and are rarely satisfactory for sterilization packaging.

b. Parallel-jaw sealers, which may be hand or foot operated, have one of the jaws heated and this presses against the opposing unheated jaw. Heat-seal packaging placed between the jaws is heated and compressed.

c. Heat-seal conveyors work in a similar manner, but items to be sealed are moved between heated elements of the conveyor.

C7.61 The seal integrity and strength is affected by the temperature, pressure and dwell time of the heat-sealing equipment.

C7.62 In order to ensure reproducible satisfactory sealing all three variables should be validated, controlled and monitored.

C7.63 Many of these heat sealers are available without a built-in timer, with no reproducible control over sealing pressure and with no indication of the operating temperature. The design of many heat sealers makes effective monitoring, calibration and adjustment of the operating conditions difficult.

C7.64 Any heat sealer which is to be used for sealing packs for sterilization should be monitored regularly for the controlling variable of temperature, pressure and dwell time. Machines which cannot be independently tested should not be used.

Overseal crimpers

C7.65 Crimping devices for the application of crimp-on overseals may be manual or automatic.

C7.66 The manual crimpers are available as hand-held devices or as bench-mounted, lever-operated machines.

C7.67 Most, if not all, of the manually operated crimping equipment available is pre-set for overseals of a particular size, or has sets of change parts to accommodate other sizes. The compressive force applied is not adjustable.

C7.68 It is essential that the crimper is only used with overseals, stoppers and containers of the pattern for which it is intended.

C7.69 Crimpers for applying foil caps to aluminium tubes for use in hot air sterilizers are also available. These are usually hydraulically operated.
Screw cappers - controlled torque

C7.70 Capping machines with a built-in, adjustable, torque limiter are available. The torque setting to be used varies with the size and type of cap and the stopper or other seal being used. The settings recommended by the manufacturer of the closure should be used.

C7.71 The calibration of the torque limiting device should be verified at regular intervals.

Ampoule sealers

Manual sealing

C7.72 Although it is possible to effectively seal an ampoule without a purpose-built ampoule sealer, it is difficult to get the correct temperature, sufficiently localised and in the required time.

C7.73 Commercially available ampoule sealers use a natural gas/compressed air (low pressure of the order of 2-3 psig) or gas/oxygen flame, in burners set either side of the ampoule.

C7.74 The ampoule stands on a support platform which is vertically adjustable to position the flames at the required position on the ampoule neck.

C7.75 The flames are positioned and adjusted so that the glass wall of the ampoule neck is just by the points of the blue cones within the flames.

C7.76 The filled ampoule is rotated in the flame.

C7.77 When the glass in the heated region of the neck melts and starts to fuse the top of the ampoule is grasped with pliers or forceps and pulled upwards in a smooth but fairly rapid movement.

C7.78 This detaches the unwanted portion of the neck leaving a fused end which should be smooth and round without any sharp pointed protrusion or a long tail of glass.

C7.79 To produce consistently successful seals requires some skill, which is only achieved through practice and experience.

C7.80 Semi-automatic and automatic ampoule sealers reproduce the same sequence of events but the whole process is automatic.

C7.81 The flame temperature, the position of the flame, the dwell time, and the timing and rate of detachment of the neck extremity all affect the quality of the seal.
C8.0 Packaging operations

Routine operation, control and monitoring

C8.1 The materials, systems, equipment and procedures used should have been evaluated for their suitability before implementation for routine use (see Chapter C6).

C8.2 The following guidance is based on the assumption that high-speed packaging machinery capable of handling large batches will not be used. When large batches are to be processed on such equipment the guidance and requirements in the Regulations and Standards applicable to commercial manufacturers should be adopted.

Documentation

C8.3 There should be written specifications for all packs giving details of both the contents and the packaging requirements.

C8.4 The order in which the contents of composite packs should be placed, to facilitate their aseptic removal from the pack, should be documented in the pack specification and the associated packing procedure.

Packaging instructions

C8.5 There should be formally authorised packaging instructions for each product, pack size and type. These should normally include or make reference to the following:

a. the name of the product;

b. either a description of its pharmaceutical form and strength, where applicable, or a list of the contents of the pack;

c. the pack size expressed as the weight or volume of the product in the final container, where applicable;

d. a complete list of all the packaging materials required including quantities, sizes and types, with the code or reference number relating to the specifications of each packaging material;

e. where appropriate, an example or reproduction of the relevant printed packaging materials, and specimens indicating where to apply any batch number, references and shelf life of the product;

f. any special precautions to be observed, including the order in which components should be assembled to facilitate aseptic removal;

g. a description of the packaging operation, including any significant subsidiary operations, and equipment, to be used;

h. details of in-process controls with instructions for sampling and acceptance limits, where applicable.
Batch packaging records

C8.6 When products are prepared in batches a batch packaging record should be kept for each batch or part batch processed.

C8.7 The record should carry the batch number and the quantity of bulk product to be packed as well as the batch number and the planned quantity of finished product that will be obtained.

C8.8 Before any batch packaging operation begins, there should be recorded checks that the equipment and work station are clear of previous products documents or materials not required for the planned packaging operations and that the equipment is clean and suitable for use.

C8.9 The information should be entered at the time each action is taken and, after completion, the record should be dated and signed.

Packaging records for single packs

C8.10 The records kept should have a sequential batch code enabling finished pack to the manufacturing's lot number for any single, including packaging, used in the composition of the pack.

Batch numbering

C8.11 All packs produced should have a sequential batch code enabling traceability and, when necessary, the recall of defective product.

C8.12 The batch code used should indicate the date of sterilization, the machine used and the process log/cycle number.

C8.13 Batch numbering with sterilizer and cycle may conveniently be done after sterilization when inspecting each pack to ensure that it has not become wet or sustained any damage.

Labelling

C8.14 Each sterile pack should be clearly labelled with a description of the pack contents and the description “sterile”.

C8.15 Normally filling and sealing should be followed as quickly as possible by labelling to ensure that no mix-ups or mislabelling can occur.

C8.16 The correct performance of any printing operation (for example, code numbers, expiry dates), whether done separately or in the course of the packaging operation, should be checked and recorded.

C8.17 The accuracy of labelling should be checked. Special care should be taken when using individual pre-printed labels and when over-printing is carried out off-line. Roll feed labels are normally preferable to cut labels, in helping to avoid mix-ups.

C8.18 When large batches of single product are being processed the correct number of bags may be labelled for each batch. On completion of the packaging operation for each batch the number of labelled bags should be reconciled with the number of products packed and any surplus bags destroyed before commencement of a different product. Any pre-stamping or labelling of bags should be controlled by documented procedures.
Checks should be made to ensure that any electronic code readers, label counters or similar devices are operating correctly.

Control of the packaging operation

When setting up a programme for the packaging operations particular attention should be given to minimising the risk of cross-contamination, mix-ups, substitutions, or mis-labelling.

Before packaging operations begin, steps should be taken to ensure that the work area and packaging equipment are clean and free from any products, materials or documents previously used, if these are not required for the current operation.

All products and packaging materials to be used should be checked on delivery to the packaging department for quantity, identity and conformity with the packaging instructions.

Containers and packaging for filling should be clean before filling; particular attention should be given to avoiding and removing any contaminants such as glass fragments and metal particles.

Control of the product during packaging should include at least checking the following:

- general appearance of the packages;
- whether the packages are complete;
- whether the correct products and packaging materials are used;
- whether the labelling, including any over-printing, is correct;
- the correct functioning of packaging equipment, for example the temperature gauge reading on heat sealing equipment.

All wrapping material used should be inspected for flaws, holes, tears, dirt, stains and other defects at the time of packaging by the operator using it.

Any of these defects should be cause for rejection of the material, which should be scrapped.

Heat-sealing equipment

Closing and sealing machines must be in good condition, properly set and maintained to the manufacturer’s specification, and closing and sealing operations should be under constant supervision.

For heat-sealing operations the critical variables of temperature, temperature uniformity, pressure, pressure uniformity, dwell time, and the characteristics of the packaging materials, for example the type, thickness and uniformity of the heat-seal adhesive, should, ideally, be verified at frequent regular intervals.

If the available equipment does not provide the facility for routine monitoring of the physical operating variables then routine monitoring of process efficacy by checking the quality of the output should be adopted.

The efficacy of the seals should be tested and proved on a regular basis, not less than daily for each heat sealer.
C8.31 As a minimum daily heat-sealing records should be kept and these should be reviewed quarterly; there should also be a quarterly check on the temperature control of each heat sealer.

Glass containers
C8.32 Because of the hazards associated with glass contamination it is essential that, if packing in glass takes place, suitable precautions are described in formal documented procedures to deal with any glass breakages which may occur.

C8.33 Equipment for handling and processing glass containers should be adequately screened to ensure that any broken glass is contained. In particular, cleaning and filling equipment must be suitably screened and it is good practice to fully enclose all conveyors between cleaning and closing.

C8.34 Conveyors for glass should not pass over areas where exposed product or components may be held.

C8.35 Suitable lidded containers to be used only for the disposal of broken glass should be provided.

QC tests
C8.36 Quantitative testing of the adequacy of packaging seals and closures requires the use of laboratory facilities and equipment not available in most hospitals.

C8.37 However, there are qualitative procedures that can be carried out which are sufficient to demonstrate a satisfactory seal, although they may be of less value in any investigation as to the cause of an unsatisfactory seal.

C8.38 These procedures are based on visual examination which can be carried out either by the operator during the various stages of the packing operation or by a QC inspector given that specific task.

Pinholes
C8.39 The performance of both porous and impermeable materials as a bacterial barrier depends on them being free from pinholes and other similar defects.

C8.40 Laboratory tests for pinholes are based on detecting the passage of a dye solution.

C8.41 However, visual examination of opaque or translucent material against a bright light is a sensitive method of detection, which may be applied in the packing room.

C8.42 The method is unsatisfactory for transparent film. However the plastic film used in pouch and reel material is typically a laminate of two films. There is a very low probability of a pinhole occurring in the same spot in both films.

Inspection of seals
C8.43 A subjective assessment may be carried out by examining and opening a number of sample packs taken from production.
C8.44 Where one of the webs being sealed is transparent the uniformity of the seal can be examined without opening the pack. In other cases it will be necessary to peel open the seal.

C8.45 In carrying out the examination the following factors should be considered:

- the appearance of the seal; it should be uniform across the entire sealed surface and should be free from creases, striations or unsealed areas;
- the seal strength; the seal should be peeled apart and attention paid to whether the force required remains constant or whether there are apparent weak spots; with practice and experience it is also possible to recognise overall increased or decreased seal strength;
- the seal characteristics; when the seal is peeled apart there should be visible evidence of the seal on both of the webs, but there should be no spitting, tearing, delamination or fibre shedding;
- the condition of the packaging, particularly in the area of the seal; excessive pressure during heat sealing may cause damage or distortion; high temperatures or prolonged dwell times may cause scorching of the paper web.

Packaging for sterile medicinal products

C8.46 Filled containers of parenteral products should be inspected individually. When inspection is done visually this should be done under suitable and controlled conditions of illumination and background.

C8.47 Operators doing the inspection should pass regular eye-sight checks, with spectacles if worn, and be allowed frequent breaks from inspection.

C8.48 When other methods of inspection are used the process should be validated and the performance of the equipment checked at intervals.

Process indicators

C8.49 A system to differentiate between processed and unprocessed items should be used.

C8.50 Single-use packaging materials may be obtained pre-printed with process indicators suitable for one or more sterilization processes.

C8.51 For other packaging materials suitable process indicators may be purchased printed onto adhesive packaging tape, adhesive patches or onto labels.

C8.52 Whichever system is chosen the process indicator should conform to the requirements of the relevant European standards (BS EN 867-1 and BS EN 867-2).

Sterile product release

C8.53 Post-sterilization it is necessary to verify that the sterilization cycle was satisfactory and check that each pack is either

- labelled with a reference to the number of the sterilizer cycle through which it was processed, or
reconciled with the load manifest for the cycle, for packs which were labelled before sterilization with a reference intended to be traceable to the cycle number.

C8.54 Packaged sterile product should be inspected after sterilization and before release to ensure that the seal or closure remains intact, and that the pack is undamaged.

C8.55 The nature of the inspection will depend upon the nature of the packaging system used.

C8.56 For example, glass ampoules may be inspected for cracks and flaws visually, by means of a dye penetration test or by means of a corona discharge crack detector.

C8.57 Whenever the integrity of the packaging is in doubt the sterilized product, or in extreme cases the sterilizer load, should be regarded as non-sterile and not released for distribution.

**Operator training**

C8.58 All operators should receive training in the documented procedures that they will be expected to carry out.

C8.59 Particular emphasis should be placed on operator dependent techniques such as the correct folding and closure of wraps.

C8.60 Training should include instruction on the correct use of equipment, inspection techniques and test methods and on the intended use of the product.

C8.61 Training should be documented and recorded and should be reviewed periodically.
C9.0 Storage and distribution

Shelf life

C9.1 Time-related expiry dates for the maintenance of sterility are widely recognised as being of little value since under artificially created worst-case storage conditions packs such as textile wrapped packs could be shown to have become contaminated within 18-30 days.

C9.2 When the products were overwrapped with a dust sheet this was extended to at least nine months, and in paper/plastic pouches was found to be at least a year.

C9.3 Maintenance of sterility depends to a great extent on the storage conditions including such factors as:

- the microbial contamination of the storage environment;
- movements of air;
- movements and behavioural standard of personnel;
- environmental temperature, relative humidity;
- moisture, such as condensation;
- location in the store, etc.

C9.4 The barrier properties of the packaging material are also a contributory factor. The general concept is that the combination of the packaging and the control exerted over storage and distribution conditions should guarantee that the contents remain sterile until opened for use.

C9.5 Some form of date coding may still form a convenient inventory control system, means of assessing the frequency of usage and for deciding whether unused packs are of a type which no longer need to be produced.

C9.6 The use of arbitrary expiry dating on packs should be replaced with batch numbering and/or manufacturing date codes which can be used to facilitate good stock rotation, based on a first-in-first-out system.

C9.7 Maintenance of sterility cannot be guaranteed once the packaging has been breached and the labelling should warn the user to verify the condition of the packaging before opening the pack for use. A warning such as “sterile unless packaging opened or damaged” is usually sufficient.

Distribution of sterilized supplies

C9.8 Trolleys used for distribution within the hospital should be covered or closed with a solid bottom shelf.

C9.9 Each article to be loaded onto a trolley or into a transit container should be inspected and handled with care; packs should not be crushed together. Cramming additional packs into too small a space will invariably result in damage.
Storage of sterile supplies

C9.10 The function of this storage area may be limited to the storage of packs produced in the SSD or may also accommodate commercially produced packs and sterile devices purchased from commercial suppliers.

C9.11 Medical equipment that has been decontaminated, disinfected, cleaned, serviced, repaired and readyfor re-issue may also be stored here.

C9.12 Sufficient space is required for loading trolleys and containers for distribution on site and for loading containers for delivery off site.

C9.13 Entry to the area should be restricted to authorised and trained personnel.

C9.14 Staff should wash their hands before entering; where no convenient washing facility is available, it may be acceptable to substitute treating clean hands with an alcohol-based hand rub for washing.

C9.15 Movement of personnel within the area should be kept to the minimum necessary.

C9.16 The floor should be cleaned regularly by damp mopping and/or vacuuming; sweeping, brushing or the use of rotary scrubbing and polishing machines should be avoided since these may disperse contamination from the floor as an aerosol.

C9.17 Shelves, trolleys, delivery carts and transit containers should be subject to regular cleaning in accordance with a documented procedure and schedule.

C9.18 Packs should be spaced on shelves with sufficient room to avoid friction or the jarring of adjacent products when one is removed.

C9.19 Rigid re-usable transit containers may be used with advantage to contain smaller packs; these containers should also be on the cleaning schedule.

C9.20 Packs dropped on the floor should be discarded or sent for re-processing, as applicable, unless they were protected by an outer dust cover, such as a polythene bag, show no visible damage to the packaging and do not contain items which could be damaged by impact.

C9.21 Storage arrangements should be orderly to facilitate efficient rotation of stocks, batch differentiation and ease of cleaning.

C9.22 Sterilized packs should be issued in rotation based on the First-In–First-Out (FIFO) principle in accordance with a documented procedure.

C9.23 Sterilized packs should be handled as little as possible.

C9.24 After sterilization it is important that packs are stored safely in a manner which will assist in preserving the sterility of the contents.

Handling sterile packs

C9.25 It is important that all personnel who will be required to handle sterile packs (porters, drivers, SSD assistants, phlebotomists, nurses, clinicians, etc)
receive appropriate training in the correct handling procedures and why they are necessary.

C9.26 Many sterile packs will contain expensive and delicate Instruments and require careful handling. All sterile packs need to be handled in a manner which will not compromise their sterile condition.

C9.27 As a minimum the following rules should apply:

a. The hands of personnel who will handle sterile packs need to be clean and dry;

b. The sterile packs need to be kept dry and must not be torn, punctured or otherwise damaged;

c. Any packs that are visibly damaged, stained or wet should be returned to the SSD for disposal or re-processing, as appropriate;

d. It should be possible to verify that the pack has been processed; this may be by means of a process indicator, or by appropriate labelling such as a sterilizer cycle number. Note that process indicators do not indicate the sterility of the pack contents, only that the pack was processed through a sterilizer;

Containers, distribution trolleys and any surfaces on which the packs will be placed must be clean and dry;

Transport and distribution

C9.28 There should be documented procedures for delivery and for the packaging, collection and return of used goods

C9.29 Containers and trolleys should be easy to clean, properly maintained and should adequately isolate the goods in transit from environmental hazards

C9.30 The cleaning procedure for bulk containers and trolleys should be documented and records should be kept of cleaning carried out

C9.31 In transit the contents of containers should be adequately identified by means, such as labels, which will not be erased in transit.

C9.32 Used goods being returned must be segregated from clean and sterile goods being delivered.

C9.33 Vehicles reserved for the delivery of clean and sterile goods should be used whenever possible. If dedicated vehicles are not used then each vehicle used must be cleaned after use for the return of used goods and before use for the transport of sterile goods.

C9.34 The cleaning procedure for the vehicle interior should be documented and records should be kept of cleaning carried out.

C9.35 As an alternative the use of sealed leakproof containers may be used for transport in either or both directions.

Storage in clinical areas

C9.36 The same principles apply as were discussed for the processed goods store
C9.37 The storage facility should be secure, easy to clean and organised to aid stock rotation (for example a double-sided cupboard filled from the back but where goods are removed from the front).

C9.38 The quantity of goods stored should be limited to those actually needed within a reasonable time period.

C9.39 The place and method of storage varies, but it should be separate accommodation, not a general store with bedpans, urinals etc.

C9.40 Storage should be segregated or, if it has to be shared, it should be with other clean and/or sterile equipment.

C9.41 A high standard of cleanliness is required and packs must be kept well away from sinks and other sites of possible contamination.

Packaging for return of used items for re-processing

C9.42 A local policy for the handling of potentially contaminated and hazardous items, and practices for safe containment during transport back to the SSD need to be established.

C9.43 All returned items should be regarded as potentially contaminated and thus infective.

C9.44 Containers for returning goods should be leak proof, securely closeable and safe to handle. The container design should include the facility for clear labelling to indicate the nature of the contents.
# Glossary of terms

<table>
<thead>
<tr>
<th>Term</th>
<th>Definition</th>
</tr>
</thead>
<tbody>
<tr>
<td>Bioburden</td>
<td>Population of viable micro-organisms on an item.</td>
</tr>
<tr>
<td>Capacity (for glass containers)</td>
<td>The internal volume at 20°C.</td>
</tr>
<tr>
<td>Closure</td>
<td>Means used to close a package where no seal is formed, for example by repeated folding to construct a tortuous path.</td>
</tr>
<tr>
<td>Closure integrity</td>
<td>The quality of the closure which ensures that it presents a microbial barrier</td>
</tr>
<tr>
<td>Final pack</td>
<td>The pack in which a medical device is sterilized. In addition to the primary pack a secondary and/or transport pack may be included.</td>
</tr>
<tr>
<td>Internal pressure resistance</td>
<td>The internal hydraulic pressure which a glass container at 20°C can withstand without breaking</td>
</tr>
<tr>
<td>Microbial barrier</td>
<td>The ability to prevent the ingress of micro-organisms.</td>
</tr>
<tr>
<td>Multi-trip container</td>
<td>A glass container which has strength characteristics sufficient for it to withstand a number of filling/use operations.</td>
</tr>
<tr>
<td>Packaging compatibility</td>
<td>The ability of the packaging material and/or system to achieve the required performance without detrimental effect on the medical device.</td>
</tr>
<tr>
<td>Packaging material</td>
<td>Any material used in the fabrication or sealing of a packaging system or primary pack.</td>
</tr>
<tr>
<td>Packaging system</td>
<td>One or more packaging materials assembled into a single unit intended as part or all of a primary pack.</td>
</tr>
<tr>
<td>Primary pack</td>
<td>The sealed or closed packaging system forming a microbial barrier enclosing the medical device, and (usually) in contact with the medical device.</td>
</tr>
<tr>
<td>Seal</td>
<td>The result of joining of layers, for example by use of adhesives or thermal fusion.</td>
</tr>
<tr>
<td>Seal integrity</td>
<td>The quality of the seal which ensures that it presents a microbial barrier.</td>
</tr>
<tr>
<td>Secondary pack</td>
<td>The pack containing one or more medical devices, each in its primary pack.</td>
</tr>
<tr>
<td>Shelf pack</td>
<td>see Secondary pack.</td>
</tr>
<tr>
<td>Shipper pack</td>
<td>see Transport pack.</td>
</tr>
<tr>
<td>Single-trip container</td>
<td>A glass container designed and manufactured to be sufficiently strong to withstand only one filling/use operation.</td>
</tr>
<tr>
<td>Terminally sterilized</td>
<td>Descriptor for medical devices which are sterilized after being completely sealed or enclosed in at least the primary pack.</td>
</tr>
<tr>
<td>Thermal shock resistance</td>
<td>The ability of a glass container to withstand a sudden temperature change without breaking.</td>
</tr>
<tr>
<td>Transport pack</td>
<td>The pack containing one or more primary and/or secondary packs intended to provide the necessary protection during transport and storage</td>
</tr>
<tr>
<td>Term</td>
<td>Definition</td>
</tr>
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<td>---------------------------------------------------------------------------</td>
</tr>
<tr>
<td>Ullage</td>
<td>That part of the contents of a container which wants for filling. Expressed in units of volume or as a percentage of the total container volume.</td>
</tr>
<tr>
<td>Unit pack</td>
<td>see Primary pack.</td>
</tr>
<tr>
<td>Vacuity</td>
<td>The free space left above the contents in a sealed container expressed as a percentage of the nominal volume of the contents.</td>
</tr>
<tr>
<td>Validation</td>
<td>Documented procedure for obtaining, recording and interpreting the data required to show that a process will comply with predetermined specifications.</td>
</tr>
</tbody>
</table>
Section D

A contract for the annual testing of sterilizers
Small power
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Description of the work

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TERM CONTRACT FOR ANNUAL TESTING OF STERILIZER

INVITATION TO TENDER - SHEET 1

Contract No ........................

* FOR TRUST/HA USE

You are invited by the above NHS Trust/Employer to submit on this form, which together with all relevant documents when completed is to be delivered to the above NHS Trust Employer by ........ am/pm on ......................... 199... the enclosed label being used.

The NHS Trust Employer do not bind themselves to accept the lowest or any tender.

IF NO TENDER IS BEING SUBMITTED ALL OF THE DOCUMENTS SHOULD BE RETURNED WITHOUT DELAY USING THE ADDRESSED LABEL WHICH SHOULD BE MARKED 'NO TENDER'.

FORM OF TENDER

TO THE ......................................, NHS TRUST/EMPLOYER

FOR THE ANNUAL TESTING OF STERILIZERS

(hereinafter referred to as 'the Employer')

1. I/We have examined the following parts of the Contract Documents:

   1. Invitation to Tender
   2. Price Schedule
   3. VAT Form
   4. Schedule of Information to be supplied by the Tenderer
   5. Abstract of Particulars
   6. General Conditions of Contract
   7. Particular Specification

and subject and in accordance with the terms and conditions contained in the Contract.

I/We offer to execute all the work described in the said documents during the contract period defined in the Conditions of Contract commencing ......................... 199... at such times as may be set forth therein or as the Employer may otherwise order, in consideration of:

A. Payment by Employer at the rates or prices I/We have inserted in the said Schedule, as detailed in Annexe A.

B. Reimbursement by the Employer of Value Added Tax to be declared to HM Custom and Excise.
INVITATION TO TENDER - SHEET 2

2. The essence of selective tendering is that the NHS Trust/Employer receive bona fide competitive tenders from all persons tendering. In recognition of this principle:

I/We certify that this is a bona fide tender, and that I/We have not fixed or adjusted the amount of the tender by or under or in accordance with any agreement or arrangement with any other person. I/We also certify that I/We have not done and I/We undertake that I/We will not do at any time before the hour and date specified for the return of this tender any of the following acts:

A. communicate to a person other than the person calling for those tenders the amount or the approximate amount of the proposed tender, except where the disclosure, in confidence, of the approximate amount of the tender was necessary to obtain insurance premium quotations required for the preparation of the tender;

B. enter into any agreement or arrangement with any other person that he shall refrain from tendering or as to the amount of any tender to be submitted;

C. offer or pay or give to pay or give any sum of money or valuable consideration directly or indirectly to any person for doing or having done or causing or having caused to be done in relation to any other tender or proposed tender for the said work any act or thing of the sort described.

In this invitation the word 'person' includes any persons and any body or association, corporate or unincorporate; and 'any agreement or arrangement' includes any transaction, formal or informal, and whether legally binding or not.

3. I/We agree that other terms or conditions of contract or any general reservations which may be printed on any correspondence emanating from me/us in connection with this tender or any other agreement resulting from this tender, shall not be applicable to this tender or to the Agreement.

Signed ....................................... in the capacity of ........................................

duly authorised to sign tenders for and on behalf of

(IN BLOCK CAPITALS) .......................................................... ..........................................................

Telex No ........................................ Fax No ........................................

Postal Address ..........................................................

Telephone No ........................................ Date ........................................ 19.

Contractor's nominated liaison officer: ..........................................................
PRICE SCHEDULE

NHS TRUST/EMPLOYER

THE WORK

1. The price in this Schedule covers the cost of working within the outside normal hours as indicated in Appendix A: Sterilizer Inventory and Unit Costs.

2. Sterilizer testing shall be carried out in accordance with the advice contained in the appropriate Appendix at the frequencies stated.

3. Value Added Tax shall be reimbursed as stated in the Tender.

4. The price inserted in this Schedule shall include:
   A. the cost of all visits;
   B. the cost of compiling reports, copying and determining tests.

Total Cost (excluding VAT) £

Signed .................................. in the capacity of ..................................

(IN BLOCK CAPITALS) .................................................................
Telex No .................................................. Fax No
Postal Address .................................................................
Telephone No .................................................. Date .................
VALUE ADDED TAX ESTIMATION FORM

NHS TRUST/EMPLOYER

Job Title - Annual Testing of Sterilizers  Contract No

To: The Chairman and Members of the NHS Trust/Employer

I/We the undersigned, hereby give our Provisional Assessment of Value Added Tax payable on positively-rated Taxable Supplies of goods and/or Services chargeable to the

<table>
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<tr>
<th>Description of Goods and/or Services</th>
<th>Value (Tax Exclusive) (£)</th>
<th>Positively Rated at: %</th>
<th>Tax (£)</th>
</tr>
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</table>

Total £ .................

Signed ........................................ Date  .................

On behalf of ........................................
**Contract No ..................**

**SCHEDULE OF INFORMATION TO BE SUPPLIED BY THE TENDERER**

**SITE ..................................................................................................................**

<table>
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<tr>
<th>SERIAL NO.</th>
<th>ITEM</th>
<th>TO BE COMPLETED BY THE TENDERER</th>
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<tbody>
<tr>
<td>1.</td>
<td>Names of Technicians allocated to the above site.</td>
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<td>2.</td>
<td>The precise details of the qualifications and experience of the above technicians.</td>
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<td>3.</td>
<td>The number of technicians available off site for unplanned or emergency work.</td>
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<tr>
<td>4.</td>
<td>The location of off site technicians who will respond to unplanned or emergency requirement.</td>
<td>OFFICE LOCATION</td>
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<td></td>
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<td>1. ..................................</td>
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<td>2. ..................................</td>
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<tr>
<td></td>
<td></td>
<td>3. ..................................</td>
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<tr>
<td>5.</td>
<td>The location from which out-of-hour call outs will be arranged.</td>
<td>OFFICE ADDRESS</td>
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</table>

Signed: ....................................... in the capacity of ......................................

on behalf of (IN BLOCK CAPITALS) .................................................................

DATE ........................................
ABSTRACT OF PARTICULARS

The following shall be read in conjunction with the General Conditions of Contract.

1. DEFINITIONS

Refer to;

1.04 The Schedule(s) shall be the Price Schedule(s) for the Annual Testing of Sterilizers listed in Appendix A.

1.05 The Employer shall be the ________________________________ NHS Trust/Health Employer

1.07 The Contract Administrator shall be ________________________________

4. CONTRACT RATES AND PRICES

Refer to;

4.01/4.02 Applies/Does not apply*

The following shall be read in conjunction with the Particular Specification of Contract.

7. SECURITY AND PUBLIC HEALTH PRECAUTIONS

Refer to;

7.01 Areas subject to special security precautions:


7.02 Areas subject to special Public Health precautions:


10 REQUISITIONING OF WORKS

Refer to;

10.1 Local liaison Personnel


* Delete whichever is not to apply
GENERAL CONDITIONS OF CONTRACT

FOR ANNUAL TESTING OF STERILIZERS
GENERAL CONDITIONS OF CONTRACT

1. DEFINITIONS

1.01 ‘The Contract’ means all documents forming the tender and acceptance thereof, together with the documents referred to therein, including these Conditions (except as set out in the Abstract of Particulars) and the Appendix. All these documents taken together shall be deemed to form one Contract.

1.02 In the case of a discrepancy between these conditions and the Annexes forming part of the Contract Document, the Provisions of these Conditions shall prevail.

1.03 In the Contract the following expressions shall, unless the context otherwise requires, have the meanings hereby respectively assigned to them;

1.04 ‘The Schedule(s)’ means the Price Schedule(s) listed in the Abstract of Particulars.

1.05 ‘The Employer’ means the NHS Trust/Employer so designated in the Abstract of Particulars.

1.06 ‘The Contractor’ means the person or persons whose tender is accepted by the Employer and his or their legal personal representatives or permitted Sub-Contractors and assigns.

1.07 ‘The Contract Administrator’ is the person nominated by the NHS Trust/Employer to act for the NHS Trust/Employer in Managing the Contract or any person for the time being acting for him/her for the purpose of the Contract. Nominated representatives are listed in the Abstract of Particulars.

1.08 ‘The Authorised User’ means the person responsible for the Management of the Hospital Department in which the Sterilizer is installed.

1.09 ‘The Work’ means the work for the performance of which the Contract provides.

1.10 ‘Unscheduled Work’ means the work carried out by the Contractor at the request of the Contract Administrator which does not form part of the Work.

1.11 ‘The Site(s) means the grounds, buildings and/or installations within or without the buildings in or at which the work is to be performed under the Contract (See Inventory - Appendix A).

1.12 ‘The Contract Period’ means the period commencing on the date indicated in the invitation to Tender and continuing until a date 5 years thereafter or until such earlier date at which the Contract may have been determined by either party in accordance with Condition 2 and 7 hereof or by the Employer in accordance with Condition 10 hereof.
1. DEFINITIONS (Continued)

1.13 The proper law of the Contract shall be English Law.

1.14 Any decision to be made by the Employer under the Contract may be made by any persons authorised to act for them for that purpose and may be made in such manner and on such evidence or information as such person or persons shall think fit.

1.15 The headings to the Conditions shall not affect the interpretation thereof.

1.16 Any notice required to be given under this Contract shall be in writing and shall be delivered or posted by recorded delivery to the last known place or abode or business of the Contractor or, if the Contractor is a Company, to the registered office of the Company, in which case the notice shall be deemed to have been duly served at the time it is delivered.

2. PERIOD OF CONTRACT AND DETERMINATION

2.01 The Contract shall remain in force for a minimum period of 1 year and a maximum period of 5 years from the date for the commencement of the Contract as stated in the Invitation to Tender, subject to the due performance by the Contractor of his obligations under the Contract and without prejudice to the specific rights of the parties of determination thereunder.

2.02 The Contract may be determined (without prejudice to the Contractor’s or Employer’s rights under Conditions 7 and the Employer’s rights under Condition 10 hereof) at the end of the 1 year minimum period or at any time thereafter provided 13 weeks notice to that effect shall have previously been given by either party.

3. PROCEDURE

3.01 Subject to the provision of the Contract, the Contractor shall carry out the Work required in accordance with the Contract and to the satisfaction of the Contract Administrator at the times set out in the Schedule or at such other times as the Employer may from time to time direct and, so as not to interfere with the normal carrying out of business of the Employer’s staff in occupation of premises in which the Work is being carried out.

3.02 The Employer may from time to time by notice in writing subject to the agreement of the Contractor (which shall not unreasonably be withheld) vary the Contract by:
3. **PROCEDURE (Continued)**

   A. The deletion from the Inventory of the name and particulars of any site and the price payable for the work in respect thereof. If the Contract price for that item is an annual price, the amount to be paid to the Contractor in respect of the work satisfactorily performed up to that date specified in such notice shall be calculated pro-rata to the annual price.

   B. The addition to or the reduction in the items of work, plan and/or equipment at any of the site(s) referred to in the said Inventory and in the event of such variation a fair and reasonable adjustment of the price payable for such items of work at that site shall be agreed with the Contractor.

4. **CONTRACT RATES AND PRICES**

   NB Conditions 4.01 and 4.02 applicable as stated in the Abstract of Particulars.

4.01 The Contract Rates and Prices quoted in the Schedule and agreed by the Employer shall be subject to adjustment on each successive anniversary of the date of commencement of the Contract Period in accordance with the formula set out below:

For this purpose, the reference in this Condition to an Index refers to the appropriate Index indicated in the Health Services Price Index for Engineering Maintenance Contracts issued by the Department of Health, Richmond House, 79 Whitehall, London, SW 1A 2NS, and ‘index numbers’ means the index numbers contained therein.

**FORMULA**

\[
X = Y \quad \frac{a}{b}
\]

Where:

- **X** = The required adjusted Contract Rate or Price
- **Y** = The Contract Rate or Price that is required to be adjusted
- **a** = The index indicated for the month during which commenced the first day of the second or subsequent years for which the revised Contract Rate or price is to be calculated.
- **b** = The Base Index for the month during which the Contract Period commenced.
4. CONTRACT RATES AND PRICES (Continued)

4.02 The Contract Rates and Prices quoted in the Schedule shall apply to all the work which is required to be carried out under the Contract in accordance with Conditions 3.01 hereof, but either party may give notice under Condition 2.02 hereof to terminate the period within which the Contract Rates and Prices are applicable with a view to negotiating a revision in the said Rates and Prices. The Employer will not, however, be obliged to consider an increase in the Contract Rates and Prices to take effect in respect of the work which is required to be carried out before the end of the first year of the Contract period, or to negotiate a subsequent increase in the Contract Rates and Prices to take effect in respect of the work which is required to be carried out within a period of 12 months following a previous increase, save in circumstances, accepted by the Employer as being exceptional.

5. ACCOUNT

5.01 Invoices shall be rendered monthly within 14 days after the end of the month to the Contract Administrator.

5.02 Payment of fixed charges for ordinary testing will be made as soon as the invoices for the month can be examined and approved by the Employer. They will only be considered for payment, however, after receipt of the test results of those Sterilizers that have been satisfactorily tested and invoiced.

5.03 Accounts for retesting or Unscheduled Work ordered by the Contract Administrator will be paid as soon as possible after examination of test results and invoices and certification by the Contract Administrator.

6. ASSIGNMENT, TRANSFER OR SUB-LETTING OF THE CONTRACT

6.01 The Contractor shall not, without the written consent of the Employer whose consent shall not unreasonably be withheld, assign or purport to assign his obligations hereunder or enter into any Sub-Contract in respect of any portion of the work.

6.02 The Contractor shall be responsible for any Sub-Contractor employed by him in connection with the Work.

6.03 The Contractor shall make good any loss suffered or expense incurred by the Employer by reason of any default of failure, whether total or partial on the part of any Sub-Contractor.
7. DETERMINATION OF THE CONTRACT DUE TO DEFAULT OR FAILURE OR CORRUPTION

7.01 If materials and workmanship of the quality and standards specified have been used in carrying out the work or any part thereof is otherwise not in accordance with the Contract and if the Contractor, having been given by the Employer a notice in writing to rectify, reconstruct or replace any defective work or a notice in writing that the work is being performed in an inefficient manner, shall omit to comply with the requirements of such notices for a period of 7 days thereafter, or, if the Contractor shall fail to carry out the work during any period stated in the Schedule or otherwise as the Employer shall have directed or required, the Employer shall have the right to;

A. i. Have such unsatisfactory materials or workmanship or uncompleted work replaced, rectified or completed by persons other than the Contractor and to recover from the Contractor any cost incurred thereby in excess of the amount which would have been payable under the Contract for such work, or

ii. Determine the Contract immediately and any costs or expenses incurred thereby, from the day of such determination until the first day thereafter upon which the Contractor, but for such determination, could have determined the Contract under Condition 2.02 hereof, shall, so far as they exceed the sums which would have been payable under the Contract for that period, be chargeable to and recoverable from the Contractor by the Employer.

B. i. If the Contractor makes a composition or arrangement with his creditors, or becomes bankrupt, or being a company makes a proposal for a voluntary arrangement for a composition of debts or scheme or arrangement to be approved in accordance with the Companies Act 1985 or the Insolvency Act 1986 as the case may be or any amendment or re-enactment thereof, or has a provisional liquidator appointed, or

has a winding-up order made, or

passes a resolution for voluntary winding-up (except for the purposes of amalgamation or reconstruction), or

under the Insolvency Act 1866 or any amendment or re-enactment thereof has an administrator or an administrative receiver appointed.
7. DETERMINATION OF THE CONTRACT DUE TO DEFAULT OR FAILURE OR CORRUPTION (Continued)

offer or give or agree to give to any person any gift or consideration of any kind as an inducement or reward for doing or forbearing to do or for having done or forborne to do any action in relation to the obtaining or execution of this or any other contract with the Employer, or for showing or forbearing to show favour or disfavour to any person in relation to this or any other contract with the Employer, or if the like acts shall have been done by any person employed by the Contractor or acting on his behalf (whether with or without the knowledge of the Contractor), or if in relation to this or any other contract with the Employer the Contractor or any person employed by him or acting on his behalf shall have committed an offence under the Prevention of Corruption Acts to 1916.

7.02 The Contractor may without prejudice to any other rights and remedies that he may possess, by notice in writing determine the Contract if the Employer has not paid within 28 days of receipt of an invoice from the Contractor any amount properly payable to the Contractor by the Employer, and having been given notice by the Contractor shall fail to comply with such notice within seven days from the service thereof.

7.03 Any dispute or different of opinion arising in respect of either the interpretation or effect of 7.02 or of the amount recoverable hereunder the Employer from the Contractor shall be decided by the Employer, whose decision on that matter shall be final and conclusive.

8. INJURY TO PERSONS : LOSS OF PROPERTY

8.01 This condition applies to any personal injury or loss of property which arises out of or in any way in connection with the execution or purported execution of the Contract.

8.02 Subject to the following provisions of the Condition, the Contractor shall:

A. Be responsible for and reinstate and make good to the satisfaction of the Employer, or make compensation for, any loss of property suffered by the Employer to which this Condition applies;

B. Indemnify the Employer and servants of the Employer against all claims and proceedings made or brought against the Employer or servants of the Employer in respect of any personal injury or loss of property to which this Condition applies and against all costs and expense reasonably incurred in connection therewith;
8. INJURY TO PERSONS: LOSS OF PROPERTY (Continued)

C. Indemnify the Employer against any payment by the Employer in order to indemnify in whole or in part a servant of the Employer against any such claim, proceedings, costs of expenses; and

D. Indemnify the Employer against any payment by the Employer to a servant of the Employer in respect of loss of property to which this Condition applies suffered by that servant of the Employer and against any payment made under any Government provision in connection with any personal injury to which this Condition applies suffered by any servant of the Employer.

8.03 If the Contractor shows that any personal injury or loss of property to which this Condition applies was not caused nor contributed to by his neglect or default or by that of his servants, agents or Sub-Contractors, or by any circumstances within his or their control he shall be under no liability under this Condition, and if he shows that the neglect of default of any person (not being his servant, agent or Sub-Contractor) was in part responsible for any personal injury or loss of property to which this Condition applies, the Contractor’s liability under this Condition shall not extend to the share in the responsibility attributable to the neglect or default of that person.

8.04 A. The Employer shall notify the Contractor of any claim or proceeding made or brought in respect of any personal injury or loss or property to which this Condition applies.

B. If the Contractor admits that he is liable wholly to indemnify the Employer in respect of any such claim or proceeding, and the claim or proceeding is not an excepted claim, he, or, if he so desires and it is agreed with the Employer his insurers, shall be responsible (subject to the condition imposed by the following sub-paragraph) for dealing with or settling that claim or proceeding.

C. If in connection with any such claim or proceeding with which the Contractor or his insurers are dealing, any matter or issue shall arise which involves or may involve any privilege or special right of the Employer (including any privilege or right in relation to the discovery or production of documents) the Contractor or his insurers shall before taking any action thereon, consult the legal adviser or the Employer and act in relation thereto as may be required by the Employer, and if either the Contractor or his insurers fail to comply with this sub-paragraph, sub-paragraph B. above shall cease to apply.

D. For the purpose of this paragraph ‘an excepted claim’ means a claim or proceeding in respect of a matter failing to be dealt with under a Government provision, or a claim or proceeding made or brought by or against a servant of the Employer.
8. INJURY TO PERSONS: LOSS OF PROPERTY (Continued)

8.05 Where any such claim or proceeding as is mentioned in paragraph B. or C. of this Condition is settled otherwise than by the Contractor or his insurers, he shall not be required to pay by way of indemnity any sum greater than that which would be reasonably payable in settlement having regard to the circumstances of the case and in particular to the damage which might be recoverable at law.

8.06 In this Condition:

A. The expression ‘loss of property’ includes damage to property, loss of profits and loss of use;

B. The expression ‘personal injury’ includes sickness and death;

C. The expressions ‘servant of the Employer’ and ‘servants of the Employer’ include persons who are servants of the Employer at the time when a personal injury or loss of property to which this Condition applies occurs, notwithstanding that they cease to be such before any payment in respect of the personal injury or loss of property is made, and, where they have ceased to be such by reason of their deaths, include their personal representatives:

D. The expression ‘Government provision’ means any statute, warrant order, scheme, regulations or conditions of service applicable to a servant of the Employer making provision for continuance of pay or for payment of sick pay, or any allowance to or for the benefit of servants of the Employer, or their families, or dependants during or in respect of sickness, injury or disablement suffered by such servants.

9. INSURANCE AGAINST INJURY TO PERSONS AND LOSS OF PROPERTY

9.01 Without prejudice to his liability to indemnify the Employer under Condition 8 the Contractor shall, throughout the Contract Period, maintain and shall cause any Sub-Contractor to maintain such insurances as are necessary to cover the liability of the Contractor or, as the case may be, of such Sub-Contractor, in respect of the matters specified in Condition 8. The insurance in respect of claims for personal injury, sickness or death of any person under a Contract of service or apprenticeship with the Contractor or the Sub-Contractor, as the case may be, and arising out of had in the course of such person’s employment, shall comply with the Employer’s Liability (Compulsory Insurance) Act 1969 and any statutory orders made thereunder or any amendment or re-enactment thereof. For all other claims to which this Condition applies the insurance cover shall be £5,000,000 (or such greater sum as the Contractor may choose) for any one occurrence or series of occurrences arising out of one event.
9. INSURANCE AGAINST INJURY TO PERSONS AND LOSS OF PROPERTY (Continued)

9.02 The Contractor shall, at the request of the Employer, produce and shall cause any Sub-Contractor to produce, for inspection by the Employer, documentary evidence that the insurances required by Condition 9.01 are properly maintained.

9.03 Should the Contractor or any Sub-Contractor make default in maintaining insurances as provided in Condition 9.01 the Employer may itself insure against any risk in respect of which the default has occurred and may charge the cost of such insurance to the Contractor.

10. DATA PROTECTION ACT

10.01 Indemnity to Employer

If during the subsistence of this Contract the Contractor or any sub-contractor, or any employee servant or agent of them, is furnished by the Employer with, or otherwise obtains (with or without the knowledge or consent of the Employer), access to confidential or personal or commercial data owned or held by the Employer upon any medium either in relation to the Employer’s own affairs or those of others, and at any time either directly or indirectly discloses or copies or makes improper use of any such data to a third party or allows a third party unauthorised access to them or if the Contractor or any sub-contractor, or any employee, servant or agent of them, is responsible for or causes the loss, damage or destruction of all or any such data, the Contractor shall be liable in damages for any loss or damage suffered by the Employer and shall indemnify the Employer against all or any claims, proceedings, costs or expenses to which the Employer may be or become liable at the suit of any third party in respect thereof.

11. ADMISSION TO THE SITE(S)

11.01 The Employer may give to the Contractor notice that such persons as it may identify whether by name, description or employment or otherwise are not to be admitted to the Site(s).

11.02 The Contractor shall take all reasonable steps to ensure that such persons are not admitted to Site(s).

11.03 Subject to the provisions of sub-paragraphs 11.01 and 11.02 above and if and when directed by the Contractor shall furnish a list of names and addresses of all persons who are or may be at any time concerned with the Work or any part thereof, specifying the capacities in which they are so concerned, and giving such other particulars as the Contract Administrator may reasonably require.

11.04 The decision of the Employer as to whether any person is to be admitted to the Site(s), and as to whether the Contractor has furnished the information or taken the steps required of him by this Condition shall be final and conclusive.
12. **ARBITRATION**

12.0 1 All disputes, differences or questions between the parties to the Contract with respect to any matter or thing arising out of or relating to the Contract, other than a matter or thing as to which the decision or report to the Employer or of any other person is by the Contract expressed to be final and conclusive shall after written notice by either party to the Contract to the other of them be referred to a single Arbitrator agreed for the purpose, or in default of such agreement to be appointed at the request of the Employer by the President of such one of the following the Employer may decide:

A. The Law Society
B. The Institution of Civil Engineers
C. The Institution of Mechanical Engineers
D. The Institution of Electrical Engineers
E. The Royal Institution of Chartered Surveyors

* (Delete as applicable)

Unless the parties otherwise agree, such reference shall not take place until after the termination of determination of the Contract, or abandonment of the Works.

12.0 2 Such reference shall in the case of the Contract being subject to English Law be deemed to be a submission to arbitration under the Arbitration Acts 1950 and 1979, or any statutory modification or re-enactment thereof.

13. **VALUE ADDED TAX**

13.0 1 The Contractor shall determine whether Value Added Tax is chargeable on any or all of the goods, and services to be supplied under this Contract, and shall add the properly calculated amount of Value Added Tax to the tax invoice or other document submitted for the supplies made, in accordance with the conditions published by HM Customs and Excise.

14. **LOCAL HEALTH BUILDING REQUIREMENTS**

14.0 1 The Contractor and his employees shall comply with all relevant local requirements for working conditions in each Health Building within the Contract Area.
15. RACIAL DISCRIMINATION

15.01 The Contractor shall not unlawfully discriminate within the meaning and scope of the provisions of the Race Relations Act 1976 or any statutory modification or re-enactment thereof relating to discrimination in employment.

15.02 The Contractor shall take all reasonable steps to ensure the observance of the preceding paragraph by all servants, employees or agents of the Contractor and all sub-contractors.

16. MENTAL HEALTH ACT

16.01 The Contractor shall take all reasonable steps to ensure the observance of the Mental Health Act 1959 as repealed by the Mental Health Act 1983 or any statutory modification or re-enactment thereof by all servants, employees or agents of the Contractor and all Sub-Contractors, e.g. 16.02 to 16.05.

16.02 Patients within these Hospitals, however they may appear and behave may be receiving treatment for mental disorder under the terms of the Mental Health Act 1983. The following regulations therefore apply to everyone working on the Hospital premises - whether engaged on the staff of the Health Employer, or by contractors working within the Hospital.

16.03 Ill treatment of patients (Section 127, Mental Health Act 1983).

“It shall be an offence for any person who is an officer on the staff of, or otherwise employed in, or who is one of the Managers or, a hospital or mental nursing home to ill-treat or wilfully to neglect a patient for the time being receiving treatment for mental disorder as an in-patient in that hospital or home; or to ill-treat or wilfully to neglect, on the premises of which the hospital or home forms part, a patient for the time being receiving such treatment there as an out-patient.”

Any person guilty of an offence under this Section shall be liable:-

(a) “On summary conviction, to imprisonment for a term not exceeding six months or to a fine not exceeding the statutory maximum, or to both”.

(b) “On conviction on indictment to imprisonment for a term not exceeding two years. or to a fine of any amount or to both”.

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16. MENTAL HEALTH ACT (Continued)

16.04 Sexual Offences - Section 128, Mental Health Act 1959 (not repealed by Mental Health Act 1983). Also Section 128(5) Sexual Offences Act 1956

“Without prejudice to Section seven of the Sexual Offences Act 1956, it shall be an offence for a man who is an officer on the staff of or is otherwise employed in, or as one of the Managers of, a hospital or mental nursing home to have unlawful sexual intercourse with a woman who is for the time being receiving treatment for mental disorder in that hospital or home, or to have such intercourse on the premises of which the hospital or home forms part with a woman who is for the time being receiving such treatment there as an out-patient”.

Any person found guilty of an offence under this Section shall be liable on conviction on indictment to imprisonment for a term not exceeding two years.

16.05 Financial Transactions.

No member of staff, or staff of Contractors working on the premises, is permitted to enter into any financial transactions or arrangements with any patient.
PARTICULAR SPECIFICATION FOR THE ANNUAL TESTING OF STERILIZERS
PARTICULAR SPECIFICATION

1. REGULATIONS

All work shall be carried out in accordance with.

1.01 All relevant Acts or Parliament, statutory instruments and regulations.

1.02 Any public health, security and conduct requirements as from time to time be issued to the Contractor by the Employer.

1.03 Any relevant Safety Regulations published by the Employer copies of which are available from the Contract Administrator.

2. COMPLIANCE WITH BRITISH STANDARDS

2.01 All work and material shall company with relevant European and British Standards and Codes of Practice.

3. OBLIGATIONS OF THE EMPLOYER

The Employer shall be responsible for:

3.01 The keeping of each item of Mechanical and Electrical Plant in such a condition that its functions in accordance with the requirements of HTM 2010, BS3970, BS2646 and BS3421.

3.02 Arranging for statutory inspections to be carried out (under a separate contract).

3.03 Maintenance of a record for each item of Mechanical and Electrical Plant in accordance with the requirements of HTM 2010.

This shall contain details of all maintenance and remedial works carried out on each item of equipment to the following standards:

A. Failures

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<th>Date</th>
<th>Symptoms of failure</th>
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B. Visits by other Contractors

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<th>Date</th>
<th>Details of Work carried out including details of tests and replacements.</th>
<th>Date and time of completion</th>
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C. Statutory Inspections

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<th>Date</th>
<th>Details of any remedial work required.</th>
<th>Signature of competent person carrying out inspection.</th>
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4. ACCESS TO SITE

4.01 The expression ‘normal working hours’ in this Contract means the hours between 0800 and 1700 Monday to Friday (except Bank and Public Holidays). All other times are referred to as ‘outside normal working hours’.

4.02 So far as practicable the Contractor shall arrange for routine visits to be made during normal working hours, if it is necessary for a routine visit to be made outside these hours the prior agreement of the Contract Administrator must be obtained. No extra payment will be made for routine visits carried out outside normal working hours unless these have been specifically requested by the Contract Administrator.

4.03 Access to the site is to be only by those routes indicated by the Contract Administrator and vehicles may only be parked in those areas designated by the Contract Administrator.

4.04 During normal working hours the Contractor’s staff must report to the Local Liaison Officer or his deputy which Plant they will be working on. On completion of their task the Contractor’s staff must on each occasion enter the necessary details in the Plant History Record and inform the Representative that they have completed their task.

4.05 Outside normal working hours the Contractor’s staff must report to the main reception desk when they must inform the duty personnel of the reason for their visit. On completion of their task the Contractor’s staff must on each occasion enter the necessary details in the Plant History Record and inform main reception desk before leaving the site.

5. HEALTH AND SAFETY

5.01 It is essential that equipment is rendered and kept safe whilst it is being worked on. Also that protective clothing and other safeguards are worn and used when necessary.

5.02 Working areas associated with sumps, pits, wells, manholes etc must be guarded and warning notices displayed. The Contractor must ensure that any of his staff required to enter a confined space are made aware of the guidance contained in the Health and Safety Executive Note GS5 ‘Entry into confined spaces’ and must follow (so far as reasonably practicable) the recommendations contained therein. Steps, ladders, equipment plan or things employed in the execution of this contract shall be adequate for their purpose and be free from defects.

5.03 The requirements of the Health and Safety at Work etc 1974 must be observed at all times.
6. **FIRE PRECAUTIONS**

6.01 The Contractor must ensure that he, his employees and sub-contractors comply with the provisions of Section 1 of the Standard Fire Precautions P5 (1980 Edition) published by Her Majesty’s Stationery Office.

6.02 All combustible refuse, eg shavings, packing materials, etc must always be collected and removed from the site as soon as practicable.

6.03 If at any time the Contractor, his employees or Sub-Contractors notice anything that they consider could be a potential fire risk they must report this to the Contract Administrator.

7. **SECURITY AND PUBLIC HEALTH PRECAUTIONS**

7.01 Certain areas are subject to special security precautions. These areas are listed in the Abstract of Particulars.

7.02 Certain areas are subject to special public health precautions. These are listed in the Abstract of Particulars.

8. **FACILITIES ON SITE**

8.01 The Employer will supply electricity, for use by the Contractor from 240 volt 13 amp socket outlets placed within reasonable reach of each item of plan at no cost to the Contractor.

8.02 The Contractor’s staff may use the toilet, washroom and canteen facilities provided for staff use at the site.

8.03 Any other facilities for the works must be provided by the Contractor.

9. **WORKMANSHIP AND MATERIALS**

9.01 The Contractor shall be responsible for providing all tools, equipment and instruments necessary for the complete execution of the work. This is to include provision of 3 sets of Huckabay Towels to the requirements of HTM 2010, Part 3, Chapter 13, Paragraph 13.39 -13.56.

9.02 The Contractor is required to provide labour of the requisite standard of workmanship at all times in connection with this Contract. The work shall be executed in a workman like manner and to the satisfaction in all respects of the Contract Administrator. If any workmanship does not so accord the same shall at the cost of the Contractor be rectified or replaced as instructed by the Contract Administrator. The Contractor shall, if required by the Contract Administrator, provide evidence of a workman’s competence.
10. **REQUISITIONING OF WORKS**

10.01 The Persons from whom the Contractor will be required to accept requisitions at attend any urgent or necessary recommissioning are listed in the Abstract of Particulars.

10.02 All requisitions for emergency action will be made by telephone to the Contractor’s office or central control point and will be confirmed in writing within 7 days by the Contract Administrator.

11. **DOCUMENTATION**

11.01 The Contractor must ensure that on each occasion his staff enter the details of any work carried out on the plant in the Plant History Record before leaving the site.

11.02 The Contractor, within 14 days of the completion of the tests, shall supply the Contract Administrator with a Test Report carried out under this contract as detailed in Appendix D, together with 3 copies.

12. **DESCRIPTION OF THE WORK**

12.01 The Contractor shall undertake annual tests as described in Appendix B - Testing Philosophy & Procedures and Appendix C - Annual Performance Tests on those Sterilizers listed in Appendix A - Sterilizer Inventory.

12.02 The Contractor shall employ persons, experience, qualified and preferably certificated to a minimum City and Guilds standard, who would be competent to perform all the required tests, documentary evidence of this shall be provided. The Employer may require the said persons to demonstrate his/her competence by performing a test laid down by the Contract Administrator, to be witnessed by Contract Administrator or his/her nominated representative, prior to the letting of the Contract or during the period of the Contract. (City and Guilds courses in Sterilizer Testing Technology are available at the N.H.S.T.A. at Eastwood Park, Falfield, Glos).

12.03 The Contractor shall demonstrate that he has all the necessary equipment which is detailed in Chapter 6, Paragraph 6.1 - 6.63 of the current edition of Health Technical Memorandum 2010 (HTM) and the means of calibrating them.

Current certification of accuracy traceable to the National Physical Laboratory will be required.
12. DESCRIPTION OF WORK (Continued)

12.04 The Contractor shall prepare a schedule of the order and time in which he would perform the tests on the Sterilizers listed in Appendix A, to be agreed by the Contract Administrator prior to the awarding of the Contract.

12.05 The Contractor will confirm his intention to perform the scheduled test with the Contract Administrator or his/her nominated representative 14 days in advance.

12.06 The Contract Administrator or his nominated representative will arrange for the Local Maintenance Engineer to be available to rectify any faults which the Contractor identifies during the test.

12.07 The Contractor shall on completion of an annual test, make a signed and dated entry in the Plant History Record that the Sterilizer complies or does not comply, with the performance requirements. In the event of non-compliance the Contractor shall notify the Contract Administrator or his local nominated representative within 24 hours.

12.08 The Contractor shall issue to the Contractor Administrator, or his/her nominated representative, within 21 days of any test being carried out, the results of the tests in a test report as demonstrated in Appendix D together with 3 copies.

12.09 The Contractor shall inspect the Plant History Records of each Sterilizer to ensure that the service maintenance records, and where appropriate, the microbiological records are kept for all routine tests and ascertain they have been performed on each Sterilizer throughout the previous year. Comments shall be included in the Test report.

12.10 The Contractor shall nominate on the “Invitation to Tender Form” Sheet 2 a person who will act for the Contractor to liaise with the Contract Administrator on all matters relating to the Contract.

12.11 The Contractor will take up any problems of the Contract with the Contract Administrator or his/her nominated representative.

12.12 The Contract Administrator or his/her nominated representative may visit any site at any time to inspect the Contractor’s test procedures and results.

12.13 The Contractor when requested, on the appropriate form (See Appendix E) will be required to retest any sterilizer that has not satisfactorily passed the annual test criteria.

Repeat tests will be paid for at not more than the cost of the test of the said Sterilizer as listed in Appendix A.

12.14 The Contractor shall carry out the retesting of Sterilizers where applicable within 2 working days of receiving the request.
STERILIZER INVENTORY AND UNIT COSTS
### Sterilizer Inventory and Unit Costs

**NHS Trust or Employer**

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<th>No.</th>
<th>Location</th>
<th>Department</th>
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<td></td>
<td>SUB TOTAL</td>
</tr>
</tbody>
</table>
TESTING PHILOSOPHY AND PROCEDURES
TESTING PHILOSOPHY & PROCEDURES

The Testing of Sterilizers required under the contract are those called for in the Health Technical Memorandum No. 2010, Part 3 (HTM 2010).

The relevant clauses required for the execution of this contract in fulfilling the procedures for annual testing are presented in full in Appendix C.

Calibration of Instruments

It is the Contractors responsibility to ensure that all instruments used in executing the work are suitably calibrated and hold current certificate of calibration clearly traceable to National Physical Laboratory, British Accreditation Service and that the test system calibration is checked immediately before and immediately after each annual test and ‘is recorded and included in each Test Report. Copies of current certificates are to be forwarded to the Contract Administrator.

Test Equipment

The relevant clauses required for compliance of equipment used for sterilizer testing are those called for in the Health Technical Memorandum No. 2010 Part 3 (HTM 2010) Chapter 6, Pages 35-44.
ANNUAL PERFORMANCE TESTS
YEARLY AND REVALIDATION TESTS

The tests are listed in the Health Technical Memorandum 2010, Part 3, Chapters 7 - 19.

The results of tests done should be recorded in the Plant History Record for each sterilizer in the form of a report as described in Appendix D.

This contract requires only the yearly tests to be carried out on those Sterilizers which are listed in HTM 2010, Part 3, Chapters 4 - 5 (Check the relevant detail in Schedule of periodic tests to establish those tests only required for yearly testing in the tables).

The Contractor shall include in his report to the Contract Administrator if he becomes aware that the daily, weekly or quarterly tests have not been satisfactorily carried out.


<table>
<thead>
<tr>
<th>STERILIZER PROCESS TYPE</th>
<th>C H A P T E R</th>
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</thead>
<tbody>
<tr>
<td></td>
<td>4</td>
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<tr>
<td></td>
<td>VALIDATION</td>
</tr>
<tr>
<td></td>
<td>TABLE</td>
</tr>
<tr>
<td>Porous Load</td>
<td>2a</td>
</tr>
<tr>
<td>Fluids</td>
<td>2b</td>
</tr>
<tr>
<td>Unwrapped Instrument and Utensil</td>
<td>2c</td>
</tr>
<tr>
<td>Dry Heat</td>
<td>2d</td>
</tr>
<tr>
<td>Low Temperature Steam and</td>
<td>2e</td>
</tr>
<tr>
<td>Low Temperature Steam and Formaldehyde</td>
<td>2e</td>
</tr>
<tr>
<td>Ethylene Oxide</td>
<td>2f</td>
</tr>
<tr>
<td>Laboratory</td>
<td>3a</td>
</tr>
<tr>
<td>Laboratory Culture Media Preparators</td>
<td>3b</td>
</tr>
</tbody>
</table>
REPORTS
REPORTS

Each annual test carried out must be fully reported in the format shown. Each report will consist of:

1. Title page with details of NHS Trust or Hospital, Department, Manufacturer, Sterilizer type, References and date of test and person(s) carrying out the test.

2. Sequence Test Sheet listing each test carried out, a brief statement on test result and any adjustments or actions taken.

3. Test Report Sheet giving detailed analysis of the test carried out with a conclusion and recommendations.

4. Test Sheets showing details of test carried out (See specimen test sheets).

NOTE: Test sheets may be replaced by suitable computer printouts providing they are authorised by Contract Administrator.

5. Associated test recorder thermocouple charts, including calibration checks, sterilizer recorder charts, and/or print-outs, Bowie/Dick sheet where applicable. All annotated and suitably identified.

6. Each reports must be suitably bound and forwarded to the Contract Administration together with 2 copies.
2. TEST SEQUENCE SHEET

................................................. NHS TRUST/EMPLOYER

<table>
<thead>
<tr>
<th>NO.</th>
<th>TEST UNDERTAKEN</th>
<th>PASS/FAIL</th>
<th>COMMENTS BRIEF STATEMENT</th>
</tr>
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<tbody>
<tr>
<td>1.</td>
<td>................</td>
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<td>2.</td>
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<td>3.</td>
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<td>4.</td>
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<td>5.</td>
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<tr>
<td>ETC.</td>
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</tr>
</tbody>
</table>

Hospital: Department: Date Tested:
Manufacturer: Ref No: Our Ref or File No:
3. TEST REPORT SHEET

........................................NHS TRUST/EMPLOYER

Hospital: Department: Date Tested:

Manufacturer: Ref No: Our Ref or File No:

1. DETAIL REPORT

Detailed report of findings as to conforming to standards, faults found, action taken, and recommendations.

2. RECORDS

HTM 2010 APPENDIX 3. Thermometric Charts/Data Logged/Summary Sheets for process type
Statement on findings of Plant History Record regarding Maintenance and Periodic Testing status.

3. CONCLUSIONS

Brief statement from above detailed report.

4. TESTER’S NAME

.............................................................

5. TESTER’S SIGNATURE

..........................................................

6. DATE

..........................................................
### 4. SPECIMEN TEST SHEETS

<table>
<thead>
<tr>
<th>Instrument</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Unwrapped Instrument &amp; Utensil Sterilizer</td>
<td>REF 46/130V</td>
</tr>
<tr>
<td>Porous Load Sterilizer</td>
<td>REF 46/129V</td>
</tr>
<tr>
<td>Fluids Sterilizer</td>
<td>REF 46/132V</td>
</tr>
<tr>
<td>Dry Heat Sterilizer</td>
<td></td>
</tr>
<tr>
<td>Laboratory</td>
<td>REF 46/133</td>
</tr>
<tr>
<td>Low Temperature Steam With and Without Formaldehyde</td>
<td></td>
</tr>
</tbody>
</table>

(The above test sheets are D.O.H. approved and are available from Printing Services, NHS Supplies Authority, South & West Division, St. Modwen Road, Parkway Industrial Estate, PLYMOUTH PL6 8LH.)

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LABORATORY - MEDIA
RETEST REQUEST FORM
STERILIZER PERIODIC TESTING

REQUEST FOR RETEST

CONTRACT NO. ........................................

Request for Retest Form No. ........................................

FROM: .............................................................................. NHS TRUST HEALTH EMPLOYER

TO: .............................................................................. CONTRACTS

Request for retesting following rectification of faults:

TRUST/EMPLOYER ................................................................
HOSPITAL ........................................................................
CLINIC ...........................................................................
STERILIZER ....................................................................
PLANT NO. ......................................................................
DEPARTMENT ....................................................................
ROOM NUMBER ..................................................................

Signature of Contracts Manager or Liaison Person: ........................................

Date of request: ........................................

Note: The retesting following any remedial works shall be carried out within three working days of receiving notice, unless requested later.
Section E

Procedures for determining the sound power generated by a sterilizer
Contents

E.1 Introduction page 175
E.4 Apparatus page 175
E.6 Test procedure page 177
E.13 Test result page 177
E.0 Procedures for determining the sound power generated by a sterilizer

Introduction

E.1 This test, to be carried out by the manufacturer of a sterilizer, is based on the test in Appendix D of BS 3970: Part 1: 1990 and in Section 23 of EN 285.

E.2 Except where otherwise stated here, the sound power levels of sterilizers are determined by the method described in BS 4196: Part 6: 1981 (equivalent to ISO 3746: 1979) The information given here is by itself not sufficient to permit the test to be carried out by personnel unfamiliar with the requirements of BS 4196.

E.3 Measurements made by this method have a standard deviation of up to 5 dB for discrete tone sources and up to 4 dB for wide-band noise sources. The uncertainties can be minimised by careful consideration of the conditions in which the test is carried out.

a. The environmental correction factor, K, depends on the relative sizes of the sterilizer and the test room and the sound absorbing qualities of the room. For a given sterilizer, the larger the room the smaller the value of K. Although EN 285 specifies that K should be less than 7 dB, this is a relatively high value and the manufacturer should aim to achieve K = 2 dB or less. This figure can normally be achieved by carrying out the test in a sufficiently large room. The assembly hall in which the sterilizer is constructed should be suitable;

b. Another source of error is the ambient background noise. Table 4 of BS 4196: Part 6 gives correction factors for different levels of background noise, but the lower the correction factor the more reliable the result will be. The correction is essentially zero if the background noise level is 10 dB or more below the level measured when the sterilizer is operating. It should be possible to achieve this on the manufacturer’s premises if the test is carried out when the factory is closed and all other plant is shut down. Steam and compressed air plant not part of the sterilizer should be run on storage during the test, with boiler feed pumps and compressors switched off.

Apparatus

E.4 Sound-level meter, complying with type 1 of EN 60651: 1994, or an integrating-averaging sound level meter complying with type 1 of EN 60804: 1994. The sound power level is determined from at least six microphone positions (Figure E1). If the sound meter has insufficient input channels, additional instruments and/or repeated operating cycles are required.

E.5 Test room, configured so that the distance between any wall or other object in the room is not less than 3 m from any reference surface (see paragraph E.6) on the sterilizer to be tested. The room in which the sterilizer is assembled may be suitable providing the conditions discussed in paragraph E3 are met.
Procedures for determining the sound power generated by a sterilizer

Figure ET Location of microphones for sound pressure test
**Test procedure**

**E.6** The test determines the A-weighted sound power using a rectangular measurement surface. The “reference surface” defined in BS 4196: Part 6 is the smallest rectangular box that just encloses the sterilizer, with a width and depth measured from the outside of the vessel lagging and a height measured from the floor to the top of the vessel lagging. The box does not include pipes and valves used to connect the sterilizer to its services.

**E.7** Determine the sound absorption area, \( A \), of the test room using the experimental method described in A.3.1.2 of BS 4196: Part 6. The method of estimation described in A.3.1.1 may be used as a check.

**E.8** Determine the environmental correction factor, \( K \), as described in A.3.1 of BS 4196: Part 6. Although EN 285 allows \( K \) to be as high as 7 dB, a figure of around 2 dB should be achievable as described in paragraph E.3a.

**E.9** Sterilizers should be regarded as “large sound sources” as defined in 7.4.3.2 of BS 4196: Part 6. The measurement distance, \( d \), should be 1.0 ± 0.1 m. Microphones should be placed on the measurement surface as described in 7.4 of BS 4197: Part 6. At least six microphones will be required.

**E.10** The test is to be carried out with all integral equipment (for example, water pumps, vacuum pumps, compressors) operating normally.

**E.11** Load the sterilizer with a full load as described in Part 3 of this HTM. If there is a choice of operation cycle, select the cycle with the highest sterilization temperature. Ensure that the pressure and flow from the steam and water services are set to levels which cause the maximum noise and are within the ranges specified for normal operation. Start the operating cycle.

**E.12** Using the procedure for measuring the rectangular measurement surface described in BS 4196: Part 6, determine the A-weighted sound power level and the peak sound power level of the sterilizer either for one complete operating cycle or for a 30-min period that contains the most prominent sounds.

**Test result**

**E.13** Record the calculated mean and peak A-weighted sound power levels in decibels to the nearest integer. Other information should be recorded in accordance with BS 4196: Part 6.

**E.14** The test should be considered satisfactory if the peak A-weight sound power level at no time exceeds the mean A-weighted sound power level by more than 15 dB.
Section F

Accommodation for ethylene oxide gas cylinders, manifolds and canisters
Contents

F.1 General page 183

F.3 Ethylene oxide cylinders page 183
  F.5 General principles

F.11 Ethylene oxide cartridges page 184
F.0 Accommodation for ethylene oxide gas cylinders, manifolds and canisters

General

F.1 For use in large sterilizers operating at above atmospheric pressure, ethylene oxide is mixed with carbon dioxide or chlorofluorocarbon. Given recent concerns about environmental issues however, the use of the latter is deprecated and is no longer in widespread use. The cylinders therefore are less hazardous than those of pure ethylene oxide.

F.2 Single-shot cartridges of pure ethylene oxide for use in sub-atmospheric pressure machines require care but in view of the modest volumes involved do not pose a major safety problem.

Ethylene oxide cylinders

F.3 Cylinders are categorised in accordance with Table F1 and, although ethylene oxide is supplied in mixture with inert gas, they should be stored under the toxic and/or corrosive and flammable category.

F.4 Cylinders may be stored with other industrial and medical gas cylinders in accommodation designed in accordance with HTM 2022.

General principles

F.5 Accommodation should be well ventilated and labelled clearly to describe the gases contained. The labelling should include details of emergency action procedures and the location of keys should be identified. Cylinder storage should be designated as a “no smoking” area and appropriate labels should be posted.

F.6 Clear and secure access is required to permit safe cylinder loading/unloading and handling with vehicular access.

F.7 The maximum temperature in the cylinder store should be that recommended by the gas supplier/manufacturer. Normally this should not exceed 38°C.

F.8 Accommodation should be free from naked flames and sources of ignition and appropriate fire extinguishing equipment should be available. Lighting protection may be necessary for isolated buildings and British Standards CP362 should be consulted.

F.9 For electrical equipment in the vicinity of the gas cylinders the recommendations of BS5345: 1976, Zone 2 classification will usually be appropriate for the open-air type of installation.

F.10 Safety equipment in the form of protection goggles, gloves and a respirator should be available inside this space and also at the point of entry.
Ethylene oxide cartridges

F.11 Sufficient secure storage within the loading area in the form of a locked cabinet is satisfactory for cartridges for use in a single day.

F.12 Additional cartridges will be required for an operational unit and external storage, for example one week’s supply, should be held externally. Small special-purpose cabins typically used for the storage of LPG containers fully protected from the elements will be appropriate.

<table>
<thead>
<tr>
<th>Group classification of gas cylinder contents</th>
<th>Medical gases</th>
<th>Non-medical gases</th>
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</thead>
<tbody>
<tr>
<td>1 Flammable</td>
<td>Cyclopropane - this is no longer manufactured</td>
<td>Acetylene LPG (e.g. propane, butane) STG (synthetic town gas) Methane, natural gas, hydrogen</td>
</tr>
<tr>
<td>2 Oxidising and/or supports combustion</td>
<td>Medical compressed air oxygen Nitrous oxide Oxygen/nitrous dioxide Oxygen/carbon dioxide Oxygen/helium mixtures</td>
<td>Compressed air oxygen Nitrous oxide Oxygen/nitrous oxide mixtures</td>
</tr>
<tr>
<td>3 Toxic and corrosive</td>
<td>Ammonia Ethylene oxide (C₂H₅O) Carbon monoxide C₂H₂O/CO₂ mixtures &gt; 6% C₂H₂O</td>
<td>Nitric oxide mixtures Sulphur dioxide Chlorine</td>
</tr>
<tr>
<td>3.1 Toxic and/or corrosive and flammable</td>
<td>Ethylene oxide/halo-carbon mixtures &lt; 15% C₂H₅O Certain conditions only - ethylene oxide/halo-carbon dioxide mixtures &lt; 6% C₂H₂O</td>
<td></td>
</tr>
<tr>
<td>3.2 Toxic and/or corrosive and oxidising</td>
<td>Ethylene oxide/halo-carbon mixtures &lt; 15% C₂H₅O Certain conditions only - ethylene oxide/halo-carbon dioxide mixtures &lt; 6% C₂H₂O</td>
<td></td>
</tr>
<tr>
<td>3.3 Toxic and/or corrosive only</td>
<td>Ethylene oxide/halo-carbon mixtures &lt; 15% C₂H₅O Certain conditions only - ethylene oxide/halo-carbon dioxide mixtures &lt; 6% C₂H₂O</td>
<td></td>
</tr>
<tr>
<td>4 Others including inert, but excluding toxic or corrosive</td>
<td>Carbon dioxide Helium</td>
<td>Carbon dioxide Nitrogen Argon Helium Halo-carbon Refrigerants</td>
</tr>
</tbody>
</table>
References and bibliography

NHS Estates publications


British and European Standards

BS6001 Sampling procedures and tables for inspection by attributes.

BS6068 Water quality.
  Part 6: Sampling.
    Section 6.5: 1991 Guidance on sampling of drinking water and water used for food and beverage processing.
    Section 6.7: 1994 Guidance on sampling of water and steam in boiler plants.

BS EN 25667 Water quality. Sampling.
  25667-1: 1994 Guidance on the design of sampling programmes. AMD 7435, 2/94.

EN 285 (draft) Sterilization. Steam sterilizers - large sterilizers.


EN 556: 1995 Sterilization of medical devices. Requirements for a device to be labelled sterile.

EN 724 (92/58310/DC) Guidance on the application of EN 29001 and EN 46001 and of EN 29002 and EN 46002 for non-active medical devices.

EN 868 Packaging materials and systems for medical devices which are to be sterilized.
  EN 868-2 (92/58622/DC) Sterilization wrap - Requirements and tests.
  EN 868-3 (92/58623/DC) Paper for use in the manufacture of paper bags (specified in Part 4 of this Standard) and in the manufacture of pouches and reels (specified in Part 5 of this Standard) - Requirements and tests.
EN 868-4 (92/58624/DC)  Paper bags - Requirements and tests.
EN 868-5 (92/58625/DC)  Heat sealable pouches and reel material manufactured from paper and plastic - Requirements and tests.
EN 868-6 (92/58626/DC)  Paper for the manufacture of packs for medical use for sterilization by ethylene oxide or irradiation - Requirements and tests.
EN 868-7 (92/58627/DC)  Adhesive coated paper for the manufacture of packs for medical use for sterilization by ethylene oxide or irradiation - Requirements and tests.
EN 868-8 (92/58628/DC)  Re-usable containers - Requirements and tests.

EN 867  Non-biological systems for use in sterilizers.
EN 867-2 (92/57872/DC)  Process indicators (Class A).

EN 980 (93/58310/DC)  Terminology, symbols and information provided with medical devices. Graphical symbols for the labelling of medical devices.

EN 10411  Terminology, symbols and information provided with medical devices. Information supplied by the manufacturer with medical devices. (Not yet available as draft for comment).


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Methods for the Examination of Waters and Associated Materials

Measurements of electrical conductivity and the laboratory determination of the pH value of natural, treated and waste waters. Department of the Environment/National Water Council Standing Committee of Analysts, HMSO. (out of print)


Mercury in waters, effluents, soils and sediments etc, additional methods 1985. Department of the Environment/National Water Council Standing Committee of Analysts, HMSO. (out of print)


Chloride in waters, sewage and effluents 1981. Department of the Environment/National Water Council Standing Committee of Analysts, HMSO. (out of print)


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The measurement of electrical conductivity and the laboratory determination of the pH value of natural, treated and waste waters 1978. Department of the Environment/National Water Council Standing Committee of Analysts, HMSO. (out of print)


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Steam boiler blowdown systems (Guidance Note PM 60). Health and Safety Executive, HMSO 1987.

Automatically controlled steam and hot water boilers (Guidance Note PM 5). Health and Safety Executive, HMSO 1989.

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Christie, JE. **Muslin vs. paper autoclave wrappers - a hospital study.** *Hospital Topics, Pt 1*, vol 35, pp 117-121; *Pt 2*, vol 35, pp 111-116 (March-April) 1957.

Duncan, MH. **Double wrapping - is it really necessary?** *Journal of the Association of Sterile Supply Administrators*, vol 1, no 2, pp 12-14, 1972.

Esty, JR and Meyer, KF. **The heat resistance of the spores B. botulinus and allied anaerobes. XI.** *Journal of Infectious Diseases*, vol 31, pp 650-663, 1922.

Favero, MS. **The dual meaning of heat activation.** *Spore Newsletter*, vol 2, no 12, pp 153-164.


Hughes, KEA, Drewett, SE and Darmady, EM. **The risk of contamination of sterile dressings packed in paper bags.** *British Hospital Journal and Social Service Review*, vol 77, pp 764-765, 781, 1967.

Hunter, CLF, Harbord, PE and Riddett, DJ. **Packaging papers as bacterial barriers.** *Symposium on Sterilization of Surgical Materials*, April 11-13, 1961.


Other publications in this series

(Given below are details of all Health Technical Memoranda available from HMSO. HTMs marked (*) are currently being revised, those marked (†) are out of print. Some HTMs in preparation at the time of publication of this HTM are also listed.)

1  Anti-static precautions: rubber, plastics and fabrics.†
2  Anti-static precautions: flooring in anaesthetising areas (and data processing rooms), 1977.
3  -
4  -
5  Steam boiler plant instrumentation.†
6  Protection of condensate systems: filming amines.†
8  -
12 -
13 -
2014 Abatement of electrical interference, 1993
16 -
18 Facsimile telegraphy: possible applications in DGHs.†
19 Facsimile telegraphy: the transmission of pathology reports within a hospital - a case study.†
2023 Access and accommodation for engineering services.*
26 Commissioning of oil, gas and dual fired boilers: with notes on design, operation and maintenance.†
2027 Hot and cold water supply, storage and mains services, 1995.
28 to 39 -
2040 The control of legionella in healthcare premises - a code of practice, 1993.
41 to 49 -
51 to 53 -
2055 Telecommunications (telephone exchanges), 1994.

Component Data Base (HTMs 54 to 70)
56 Partitions, 1989.
57 Internal glazing, 1995.
58 Internal doorsets, 1989.
59 Ironmongery;†
60 Ceilings, 1989.
61 Flooring.*
63 Fitted storage systems, 1989.
64 Sanitary assemblies.*
65 Health signs.*
67 Laboratory fitting-out system, 1993.
68 Ducts and panel assemblies, 1993.
70 Fixings, 1993.
71 Materials management modular system.*
72 to 80 -

Firecode
81 Firecode: fire precautions in new hospitals.*
81 Supp 1 1993.
82 Firecode: alarm and detection systems, 1989.
85 Firecode: fire precautions in existing hospitals, 1994.
87 Firecode: textiles and furniture, 1993.
88 Fire safety in healthcare premises: guide to fire precautions in NHS housing in the community for mentally handicapped/ill people, 1986.

New HTMs in preparation
2024 Lifts
2030 Washers for sterile production

Health Technical Memoranda published by HMSO can be purchased from HMSO bookshops in London (post orders to PO Box 276, SW8 5DT), Edinburgh, Belfast, Manchester, Birmingham and Bristol, or through good booksellers. HMSO provide a copy service for publications which are out of print; and a standing order service.

Enquiries about Health Technical Memoranda (but not orders) should be addressed to: NHS Estates, Department of Health, Marketing Unit, 1 Trevelyan Square, Boar Lane, Leeds LS1 6AE.
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1 Trevelyan Square, Boar Lane, Leeds LS1 6AE.
Telephone 0113 254 7000.

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Estatecode - user manual for managing a health estate. Includes a recommended methodology for property appraisal and provides a basis for integration of the estate into corporate business planning. HMSO

Concode - outlines proven methods of selecting contracts and commissioning consultants. Reflects official policy on contract procedures. HMSO

Works Information Management System - a computerised information system for estate management tasks, enabling tangible assets to be put into the context of servicing requirements. NHS Estates

Health Building Notes - advice for project teams procuring new buildings and adapting or extending existing buildings. HMSO

Health Guidance Notes - an occasional series of publications which respond to changes in Department of Health policy or reflect changing NHS operational management. Each deals with a specific topic and is complementary to a related HTM. HMSO

Health Facilities Notes - debate current and topical issues of concern across all areas of healthcare provision. HMSO

Firecode - for policy, technical guidance and specialist aspects of fire precautions. HMSO


Model Engineering Specifications - comprehensive advice used in briefing consultants, contractors and suppliers of healthcare engineering services to meet Departmental policy and best practice guidance. NHS Estates

Quarterly Briefing - gives a regular overview on the construction industry and an outlook on how this may affect building projects in the health sector, in particular the impact on business prices. Also provides information on new and revised cost allowances for health buildings. Published four times a year; available on subscription direct from NHS Estates. NHS Estates

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